

# The SuperCable: *Dual Delivery of Chemical and Electric Power*

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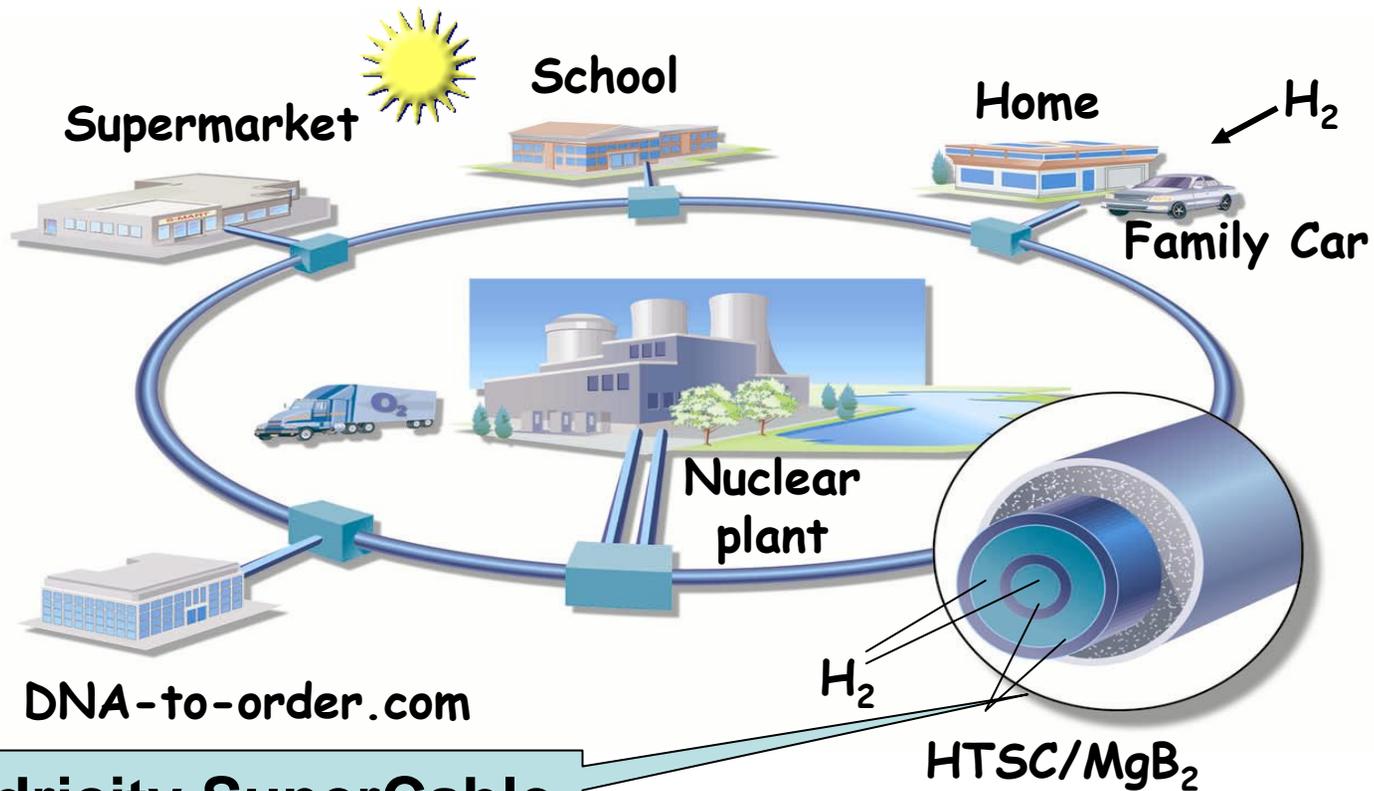
DOE Superconductivity Program Peer Review

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Poster Presentation

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# SuperCity



**Hydricity SuperCable**

P.M. Grant, *The Industrial Physicist*, Feb/March Issue, 2002

*Concept originally presented at the 2000 Peer Review*

# SuperCities & SuperGrids

*A Symbiosis of*

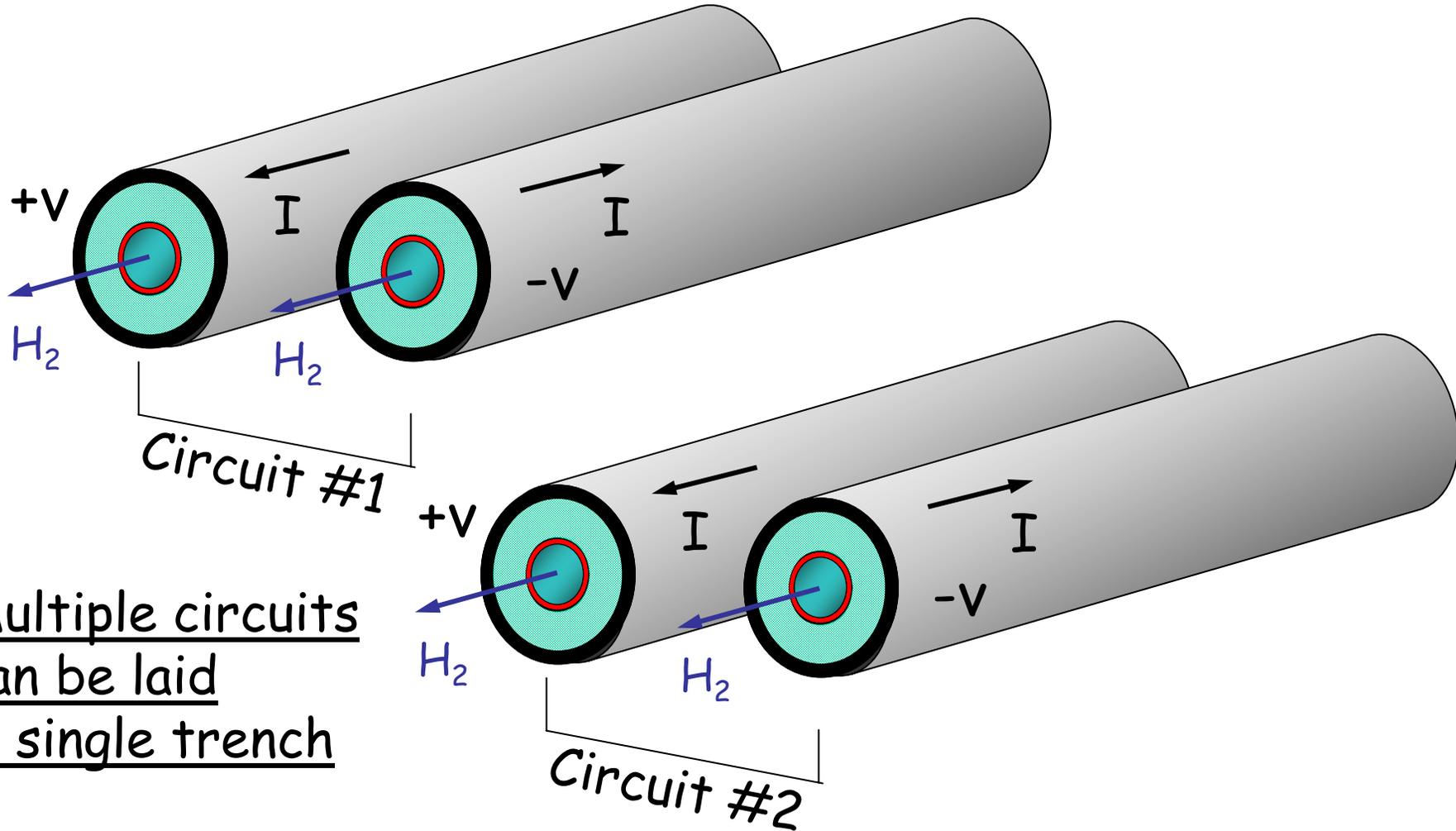
**Nuclear/Hydrogen/Superconductivity**

***Technologies supplying Carbon-free,  
Non-Intrusive Energy for all Inhabitants  
of Planet Earth***

# “Boundary Conditions”

- Givens
  - Energy Efficiency
  - Recyclables
- Off-the-Table: Eco-invasive Generation
  - Fossils
    - Carbon Sequestration
  - Baseline Renewables
    - “Farms” – Wind, Solar, Biomass
- On-the-Table
  - Nuclear (undergrounding)
  - Solar Roofs
  - Urban/Agro Biomass

# “Hydricity” SuperCables

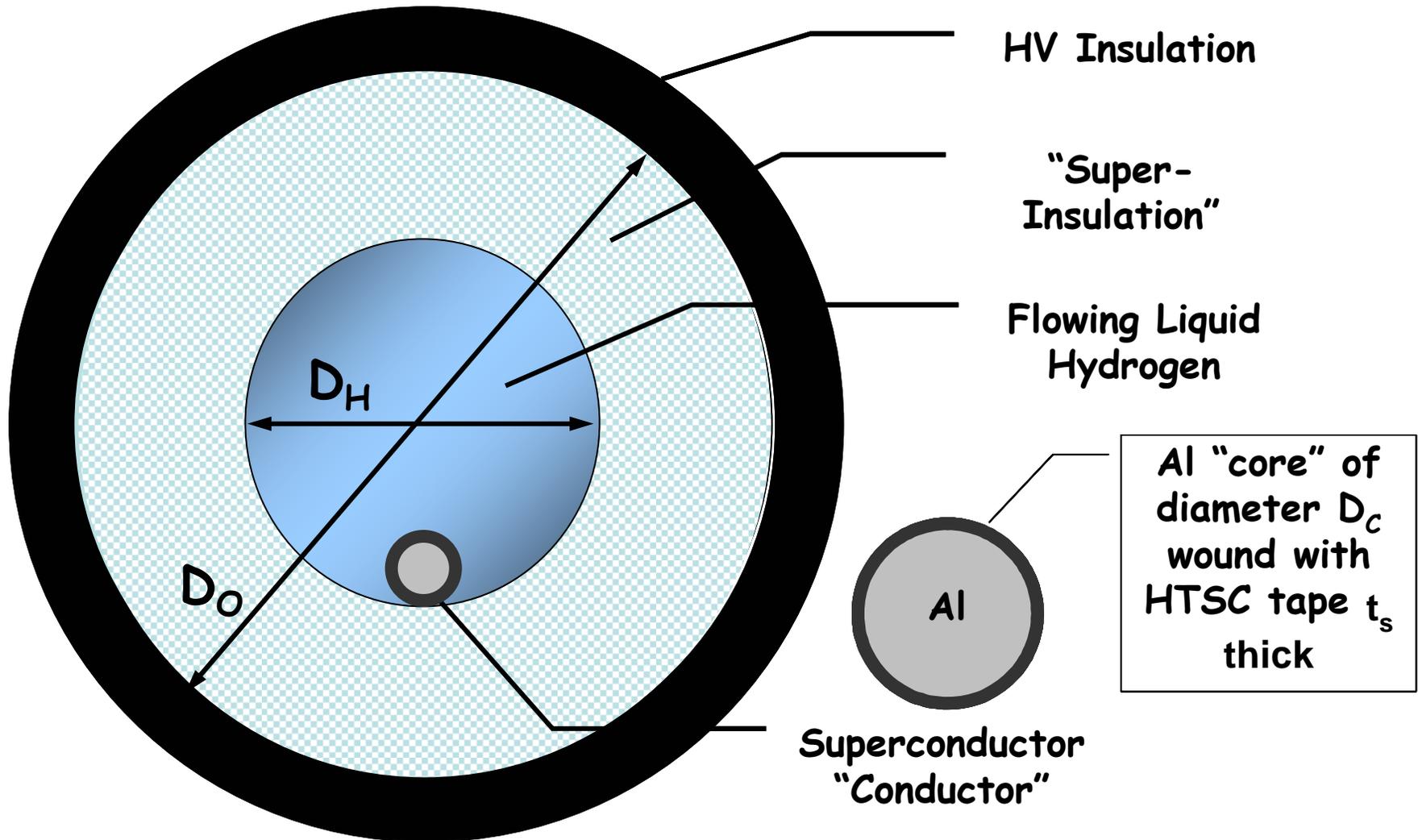


Multiple circuits  
can be laid  
in single trench

# Why Mono-Axial and Not Coax?

- Simple Design – Cheaper
- Room temperature dielectric – no cryo – dielectrics – wide separation of pole to pole potential
- Simpler design and separate placement of “accessories” (joints & terminations)
- Allows for independent (& redundant) cooling and pumping stations.
- Easy to take one pole out for service and use earth return (at lower power)
- Probably easier to handle faults – parallel normal metal shunt on each pole.
- Better suited to large scale projects – opportunity for on-site “construction kits.”

# SuperCable RTD Monopole



# Power Flows

$$P_{SC} = 2|V|JA_{SC}, \text{ where}$$

Electricity

$P_{SC}$  = Electric power flow

$V$  = Voltage to neutral (ground)

$J$  = Supercurrent density

$A_{SC}$  = Cross-sectional area of superconducting annulus

$$P_{H_2} = 2(Q\rho vA)_{H_2}, \text{ where}$$

Hydrogen

$P_{H_2}$  = Chemical power flow

$Q$  = Gibbs  $H_2$  oxidation energy (2.46 eV per mol  $H_2$ )

$\rho$  =  $H_2$  Density

$v$  =  $H_2$  Flow Rate

$A$  = Cross-sectional area of  $H_2$  cryotube

# Power Flows: $5 \text{ GW}_e / 10 \text{ GW}_{th}$

## Electrical Power Transmission (+/- 25 kV)

Power ( $\text{MW}_e$ )	Current (A)	HTS $J_c$ ( $\text{A}/\text{cm}^2$ )	$D_c$ (cm)	$t_s$ (cm)
5,000	100,000	25,000	3.0	0.38

HV Insulation

"Super-Insulation"

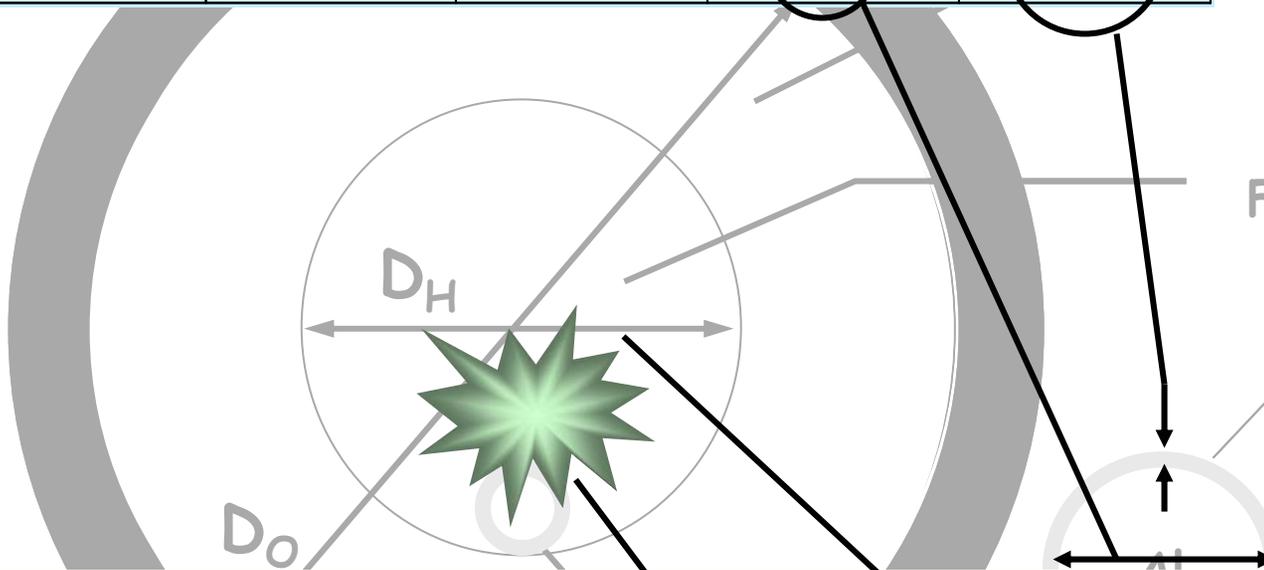
Flowing Liquid Hydrogen

Al "core" of diameter  $D_c$  wound with HTSC tape  $t_s$  thick

## Chemical Power Transmission ( $\text{H}_2$ at 20 K, per "pole")

Power ( $\text{MW}_{th}$ )	$D_H$ -effective (cm)	$\text{H}_2$ Flow ( $\text{m}/\text{s}$ )	$D_H$ -actual (cm)
5,000	40	4.76	45.3

or



# Thermal Losses

$$W_R = 0.5\varepsilon\sigma (T_{\text{amb}}^4 - T_{\text{SC}}^4), \text{ where}$$

$W_R$  = Power radiated in as watts/unit area

$$\sigma = 5.67 \times 10^{-12} \text{ W/cm}^2\text{K}^4$$

$$T_{\text{amb}} = 300 \text{ K}$$

$$T_{\text{SC}} = 20 \text{ K}$$

$\varepsilon = 0.05$  per inner and outer tube surface

$$D_{\text{SC}} = 10 \text{ cm}$$

$$W_R = 3.6 \text{ W/m}$$

Radiation  
Losses

Superinsulation:  $W_R^f = W_R/(n-1)$ , where

$n$  = number of layers

Target:  $W_R^f = \underline{0.5 \text{ W/m}}$  requires ~10 layers

Other addenda (convection, conduction):  $W_A = \underline{0.5 \text{ W/m}}$

$$W_T = W_R^f + W_A = \underline{1.0 \text{ W/m}}$$

# Heat Removal

$$dT/dx = W_T / (\rho v C_p A)_{H_2}, \text{ where}$$

$dT/dx$  = Temp rise along cable, K/m

$W_T$  = Thermal in-leak per unit Length

$\rho$  =  $H_2$  Density

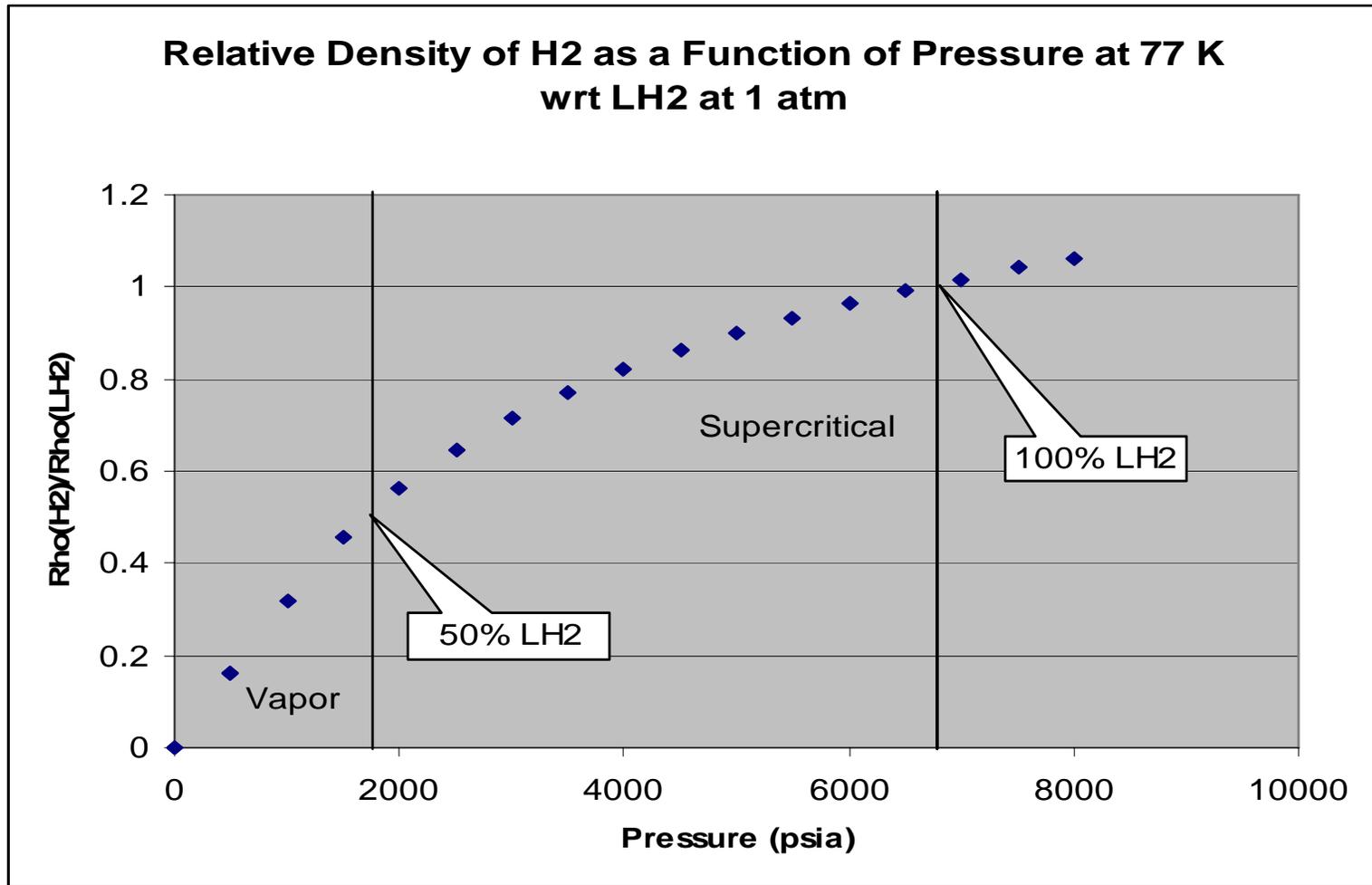
$v$  =  $H_2$  Flow Rate

$C_p$  =  $H_2$  Heat Capacity

$A$  = Cross-sectional area of  $H_2$  cryotube

Take  $W_T = 1.0 \text{ W/m}$ , then  $dT/dx = 1.89 \times 10^{-5} \text{ K/m}$ ,  
Or, 0.2 K over a 10 km distance

# Hydrogen Energy Content



***H<sub>2</sub> Gas at 77 K and 1850 psia has 50% of the energy content of liquid H<sub>2</sub> and 100% at 6800 psia !!!***

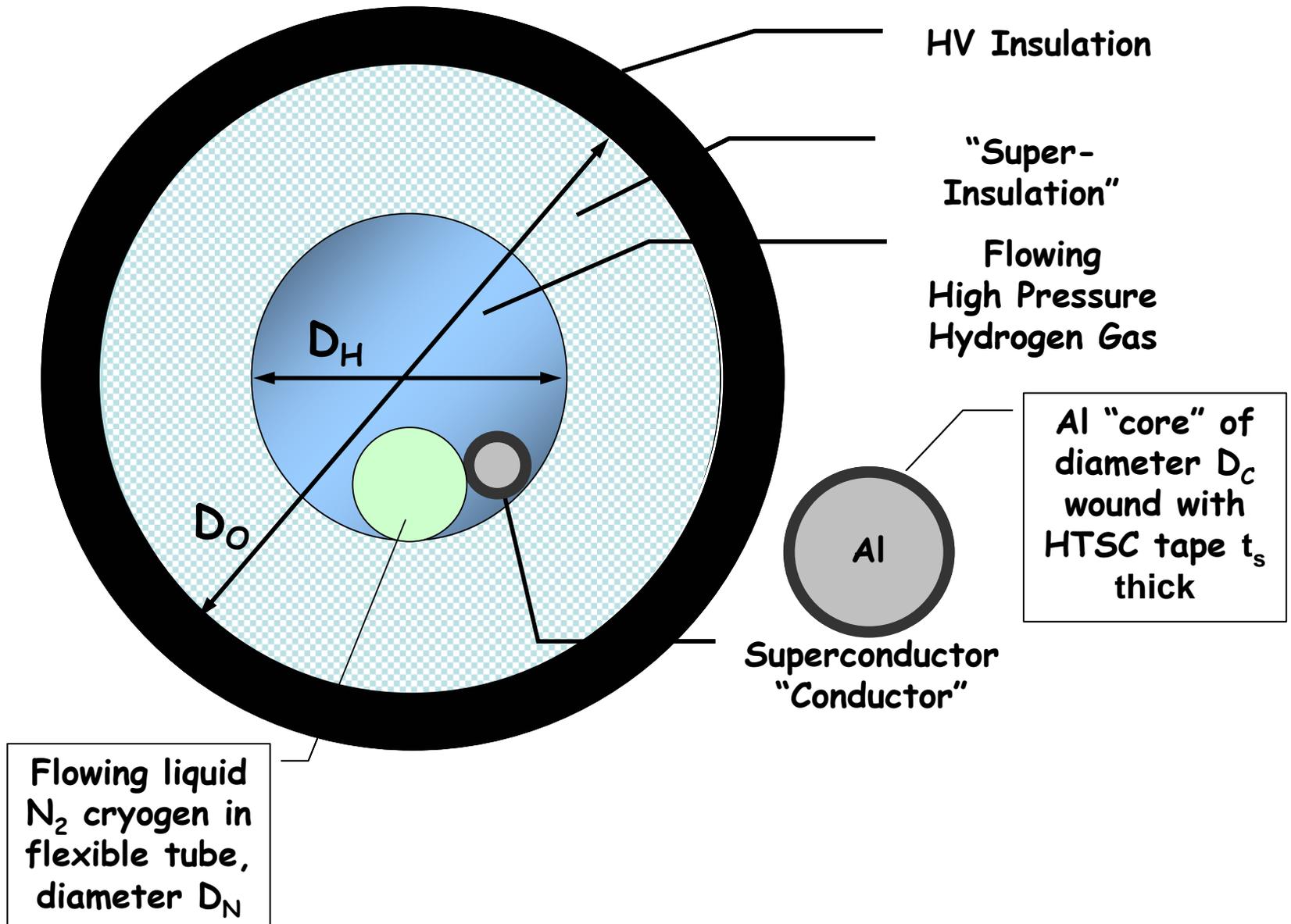
# SuperCable H<sub>2</sub> Storage

<u><i>Some Storage Factoids</i></u>	Power (GW)	Storage (hrs)	Energy (GWh)
TVA Raccoon Mountain	1.6	20	32
Alabama CAES	1	20	20
Scaled ETM SMES	1	8	8

**One Raccoon Mountain = 13,800 cubic meters of LH<sub>2</sub>**

**LH<sub>2</sub> in 10 cm diameter, 250 mile bipolar SuperCable  
= Raccoon Mountain**

# “Hybrid” LN<sub>2</sub>/GH<sub>2</sub> SuperCable



# Fluid Properties Comparison of Liquid to Gaseous Hydrogen Transporting 500 MW<sub>t</sub> in a 10-cm Diameter Pipe

<b>T</b> °K	<b>P</b> psia	<b>ρ</b> kg/m <sup>3</sup>	<b>μ</b> μPa·s	<b>μ<sup>2</sup>/ρ</b> ndyne	<b>V</b> m/s	<b>Re</b> 10 <sup>6</sup>
20	14.7	70.8	13.6	261	4	2.08
77	1850	35.4	5.6	87	8	5.06

$$Re = \rho V D / \mu \approx \frac{\text{Inertial Forces}}{\text{Viscous Forces}}$$

*Thus, it takes only 0.5 dynes “push” on an object with the above Reynolds Numbers on the gas to overcome viscous forces exerted by the given fluid*

# Fluid Friction Losses

$$p_{loss} = \lambda (l / d_h) (\rho v^2 / 2)$$

where

$p_{loss}$  = pressure loss (Pa, N/m<sup>2</sup>)

$\lambda$  = friction coefficient

$l$  = length of duct or pipe (m)

$d_h$  = hydraulic diameter (m)

$$W_{loss} = M P_{loss} / \rho,$$

Where  $M$  = mass flow per unit length

$P_{loss}$  = pressure loss per unit length

$\rho$  = fluid density

$$1 / \lambda^{1/2} = -2,0 \log_{10} [ (2,51 / (Re \lambda^{1/2})) + (\varepsilon / d_h) / 3,72 ]$$

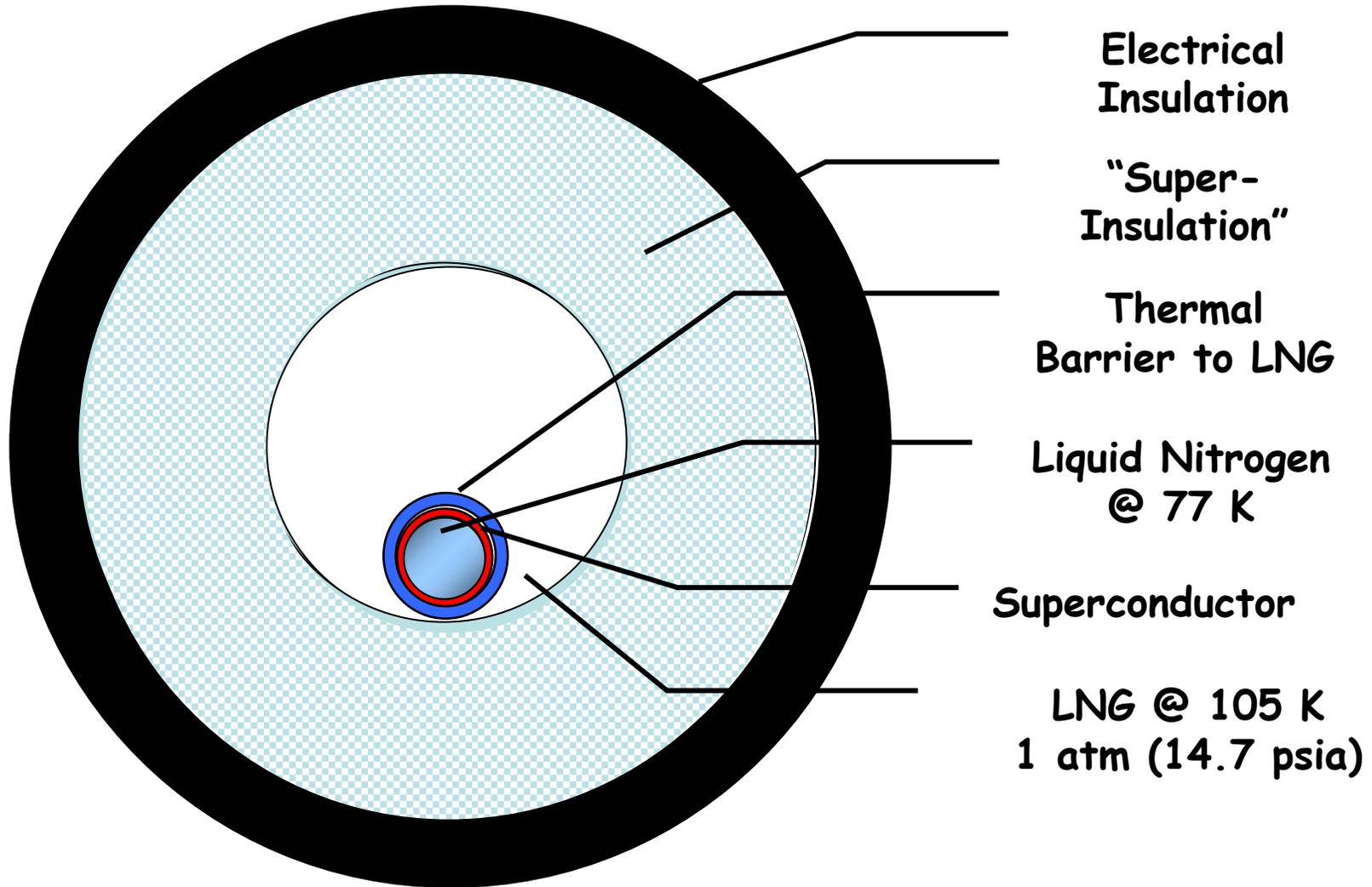
$\varepsilon = 0.015$ mm (stainless steel)	
	$W_{loss}$ (W/m)
22 K	0.72
77 K	1.30

# SuperCables & Gas Pipelines

- Methane will be the “fossil fuel of choice” for the next 25 years and many long distance pipelines (such as the Mackenzie Valley Project) and LNG seaports will be built.
- 25 – 30% will be turned into electricity near the pipeline terminus.
- Alternatively, electricity can be generated at the wellhead or dock and it and methane co-transported on a LNG hybrid SuperCable to the end user.
- When the natural gas is depleted, HTGCR nuclear plants can be built at the well and dock sites to produce hydrogen and electricity and the delivery infrastructure will be already in place.



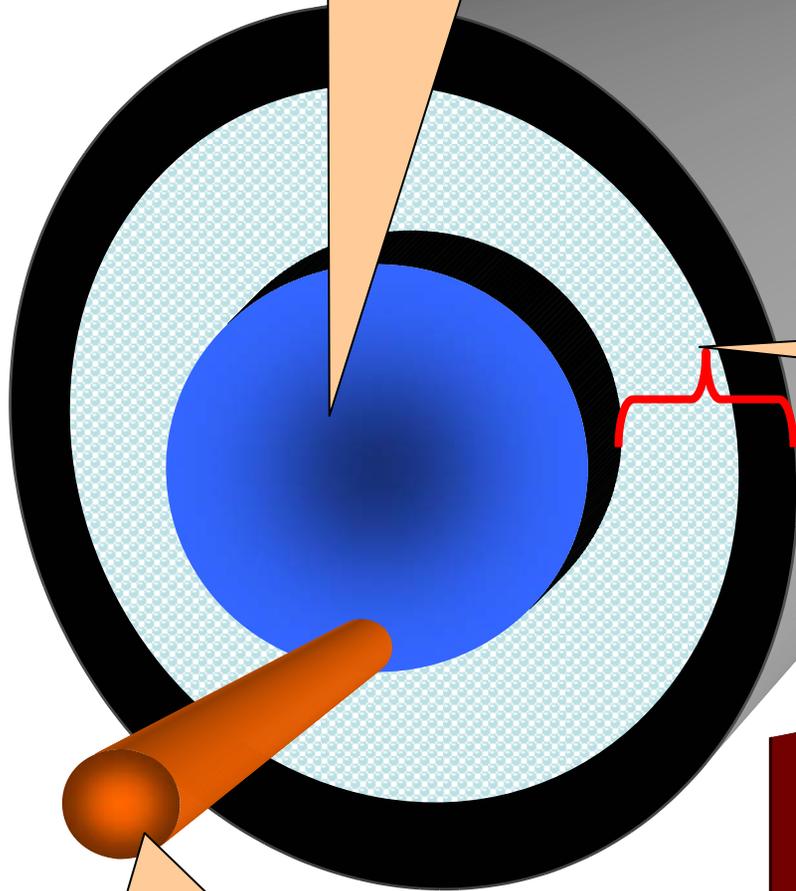
# LNG/LN<sub>2</sub> “Hybrid” SuperCable



# Construction

- Housed in trenches/tunnels for safety/security
- 20 – m rigid pre-fabed “husks” for transport by truck/barge/copter to construction site – straight or with large radius of curvature
- Superinsulation volume of each husk under “permanent” vacuum
- Ends of husk contain thermal barrier to suppress heat in-leak and bellows on inner cylinder for thermal expansion to enable jointing to neighbors.
- 1 km of pre-fabed HTSC conductor threaded from spool and loosely laid through 50 joined husks, then spliced – cooling and pumping stations every 5 km.

Open Cylindrical Tube for  
 $\text{LH}_2$  ( $\text{GH}_2$ , LNG) Flow

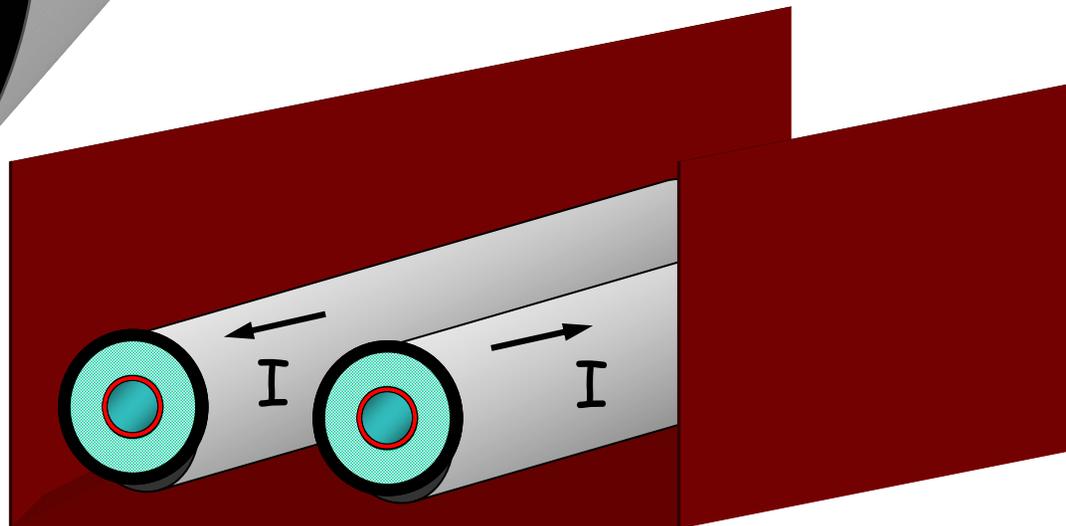


20 m Rigid Annular "Husk"  
containing HV dielectric &  
thermal "superinsulation"

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50 Connected Sections/km

1 km Threaded Continuous  
Flexible Superconducting  
Conductor ("solid" or with  $\text{LN}_2$ )



# Inverter/Converter Station Design

- Low voltage, high current
  - Parallel IGBTs?
  - 16" wafers?
  - Cryo-bipolars?
  - Fault tolerant (inverter capable of dumping fault energy into ac grid)
- “Zero Ripple Factor”
  - Necessary to reduce ac losses
  - Cable distributed reactance may aid
- Power flow management thru voltage control
  - Maintain constant current
  - New design paradigm wrt to conventional hvdc

# Additional Resources

- More information and background on the SuperCable and SuperGrid concepts can be found at
  - <http://www.w2agz.com/PMG%20SuperGrid%20Home.htm>
- A PDF copy of this poster can be downloaded from
  - <http://www.w2agz.com/Documents/2005%20PR%20SuperCable%20Poster.pdf>
- Portions of this poster will be amplified upon in two invited papers at the upcoming CEC – ICMC and PacRim 6 conferences
  - **“Cryo-Delivery Systems for the Co-Transmission of Chemical and Electrical Power,”** <http://www.cec-icmc.org/techindiv.asp?PaperNumber=C1-I-01>
  - **“System, Construction and Integration Issues for Long Distance, High Capacity, Ceramic HTSC dc Cables,”** [http://ocms.acers.org/abstract\\_action.asp?confid=32&sympid=422&sessid=3117](http://ocms.acers.org/abstract_action.asp?confid=32&sympid=422&sessid=3117) (click on Abstract List)