

# Cryo-Delivery Systems for the Co-Transmission of Chemical and Electrical Power

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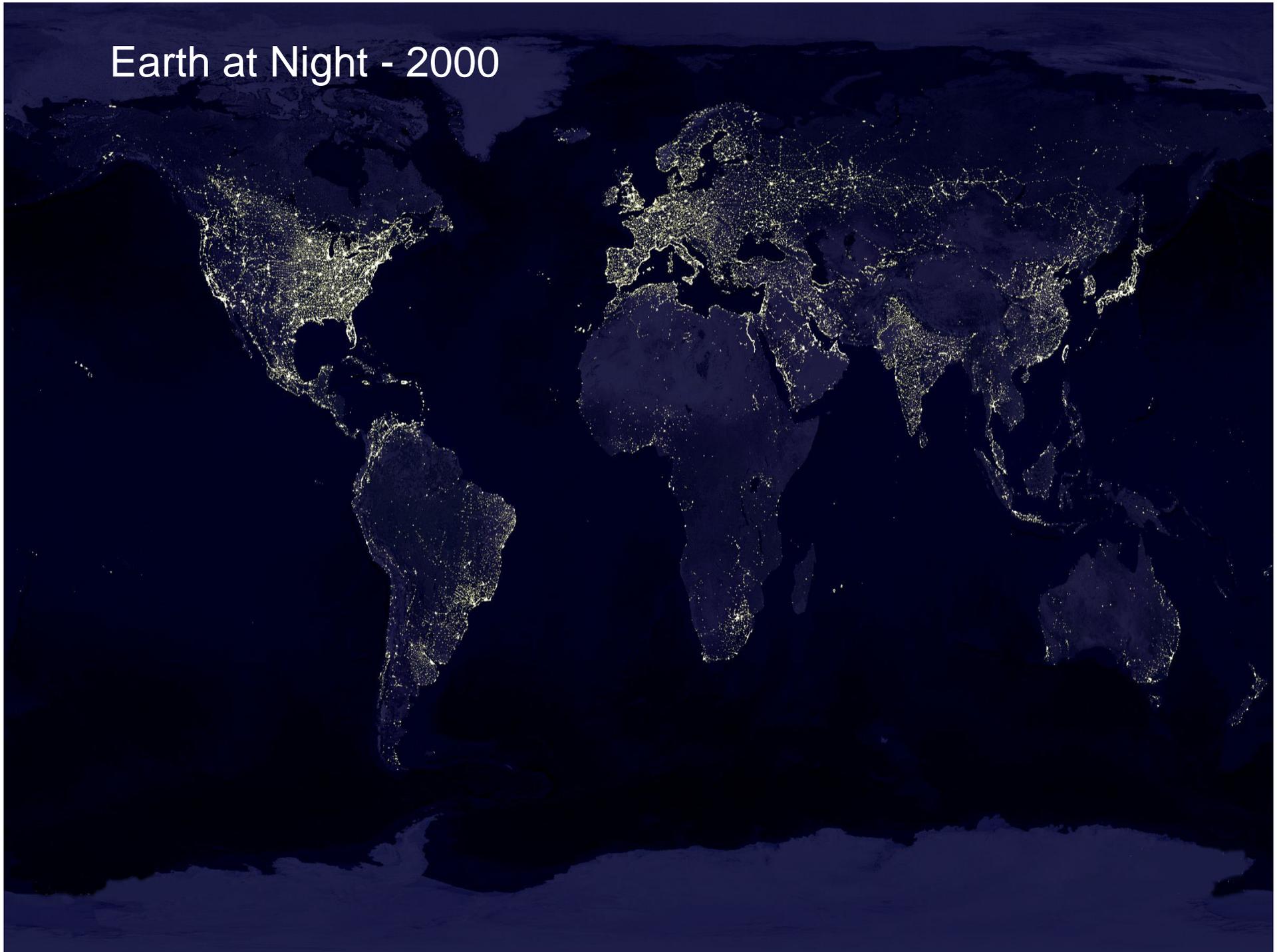
CEC - ICMC 2005

29 August - 2 September 2005, Keystone, CO

Paper C1-101, Cryofuels Session 30 August 2005, 10:30 AM

[www.w2agz.com/cec-icmc05.htm](http://www.w2agz.com/cec-icmc05.htm)

# Earth at Night - 2000



# The 21<sup>st</sup> Century Energy Challenge

*Design a communal energy economy to meet the needs of a densely populated industrialized world that reaches all corners of Planet Earth.*

*Accomplish this within the highest levels of environmental, esthetic, safe, reliable, efficient and secure engineering practice possible.*

*...without requiring any new scientific discoveries or breakthroughs!*

# Its Solution

*A Symbiosis of*

*Nuclear/Hydrogen/Superconductivity*

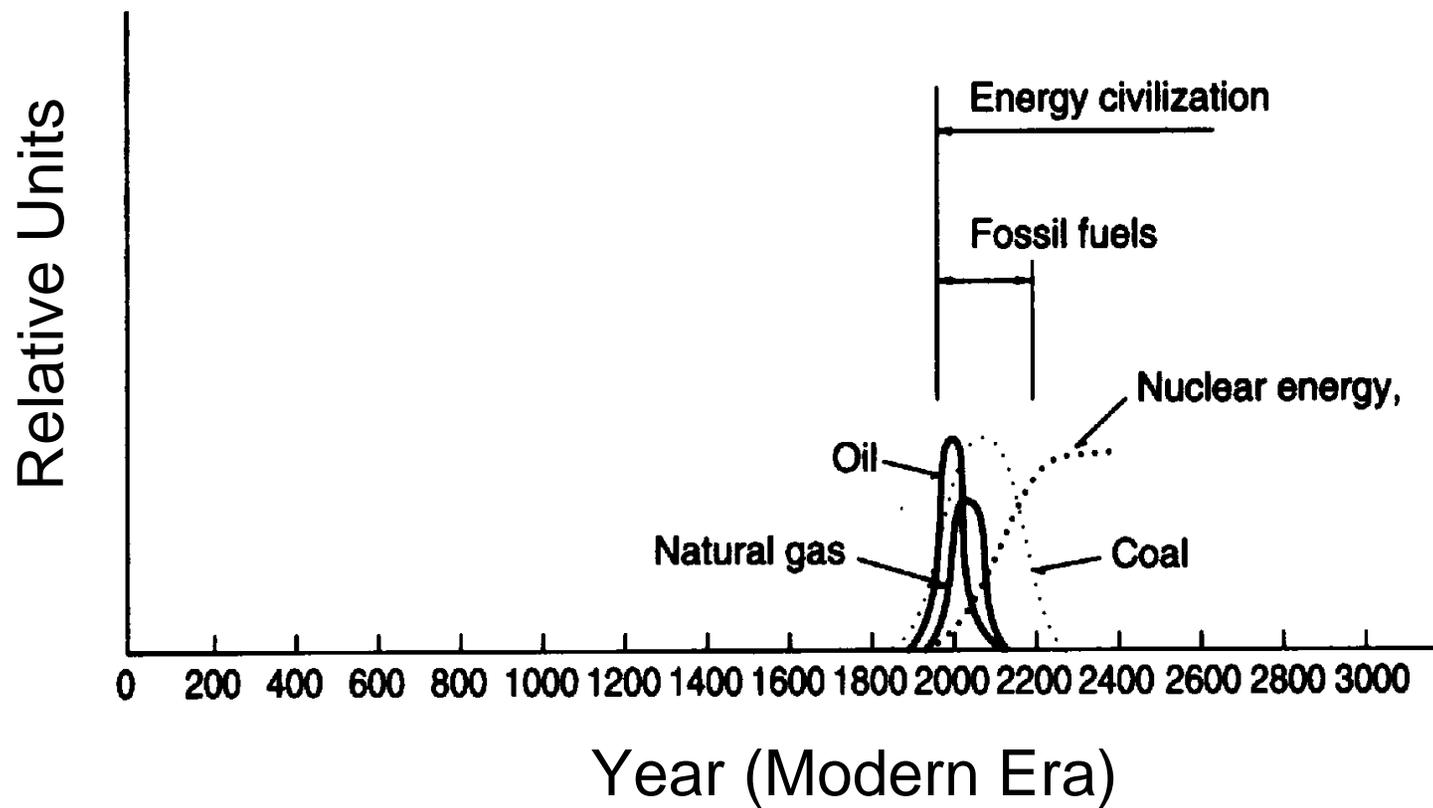
*Technologies supplying Carbon-free,  
Non-Intrusive Energy for all  
Inhabitants of Planet Earth*

SuperCities & SuperGrids

*SuperCables !*

# Past & Future Energy Supply

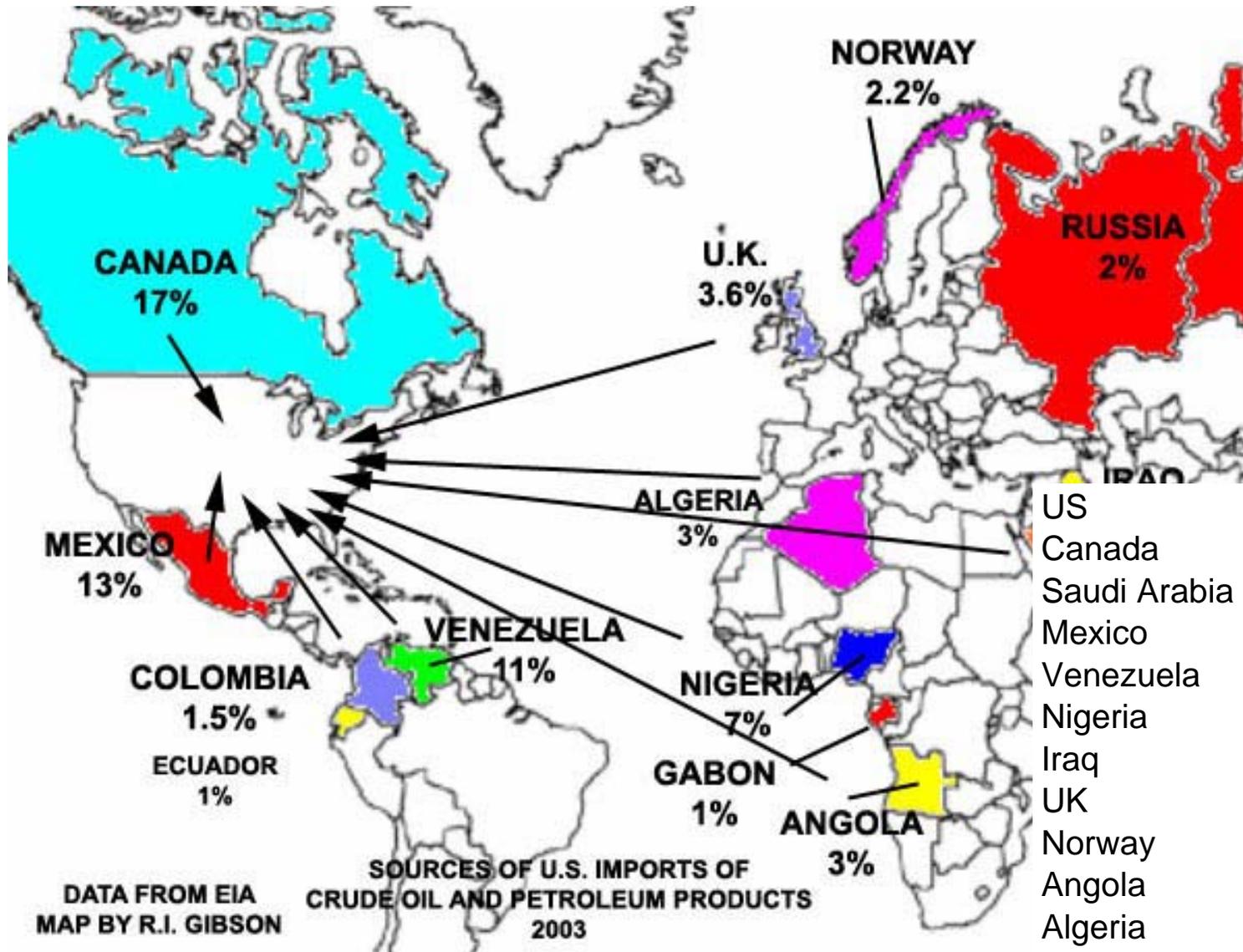
**Fig. 1 Production Volume of Energy Resources**



# US Energy Consumption (2001)

Energy Source	Percentage of total
Petroleum	42%
Coal	24%
Natural Gas	20%
Nuclear	8%
Hydro power	2%
Solar, Wind, etc.	2%

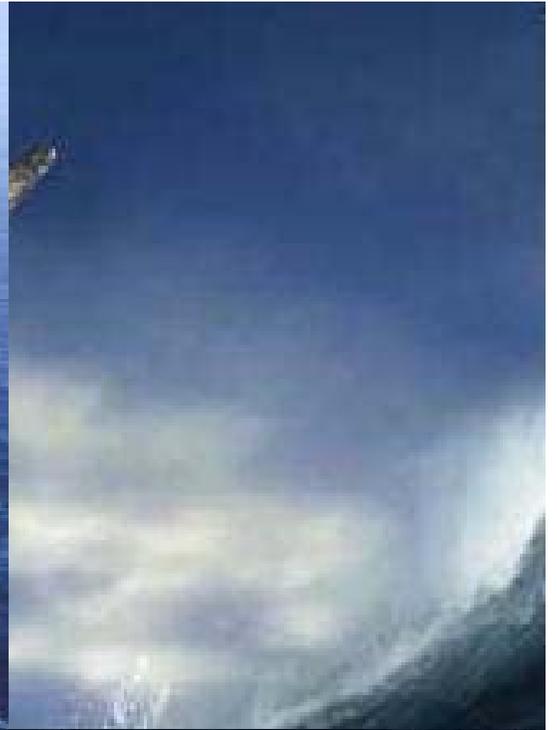
# US Oil Imports (2003)



DATA FROM EIA  
MAP BY R.I. GIBSON

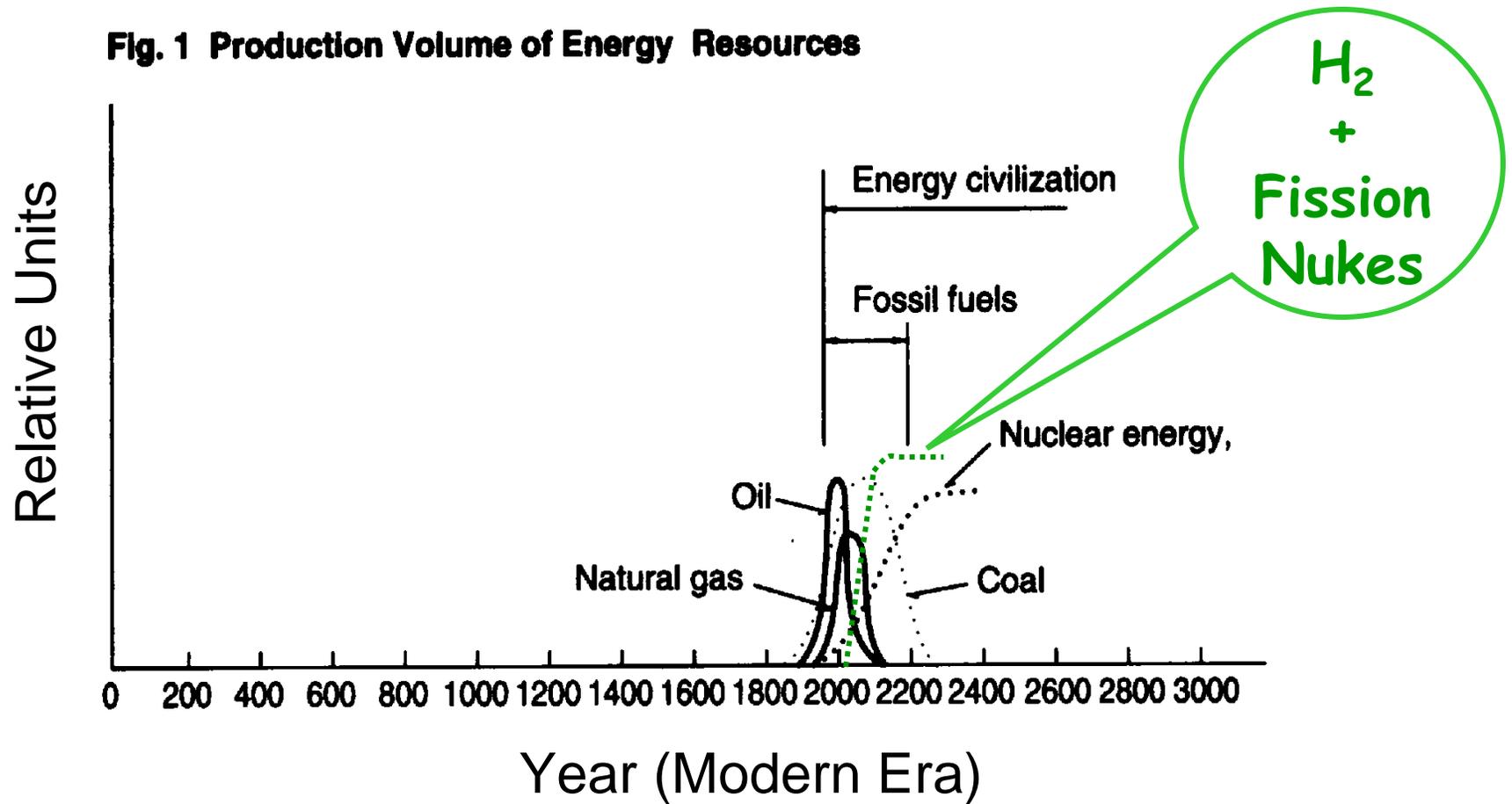
SOURCES OF U.S. IMPORTS OF  
CRUDE OIL AND PETROLEUM PRODUCTS  
2003

US	39%
Canada	13%
Saudi Arabia	10%
Mexico	10%
Venezuela	9%
Nigeria	4%
Iraq	4%
UK	3%
Norway	3%
Angola	2%
Algeria	2%
Other	2%

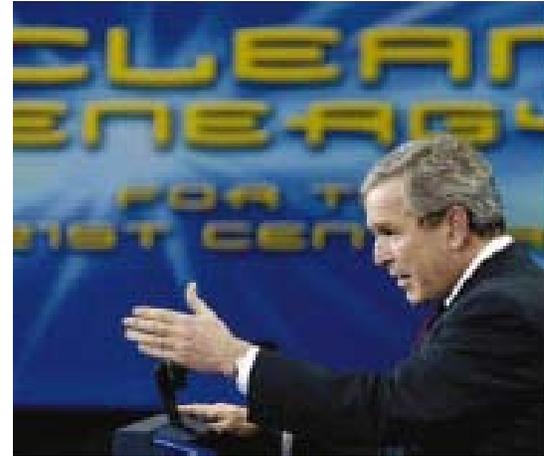


# Past & Future Energy Supply

Fig. 1 Production Volume of Energy Resources



# The Hydrogen Economy



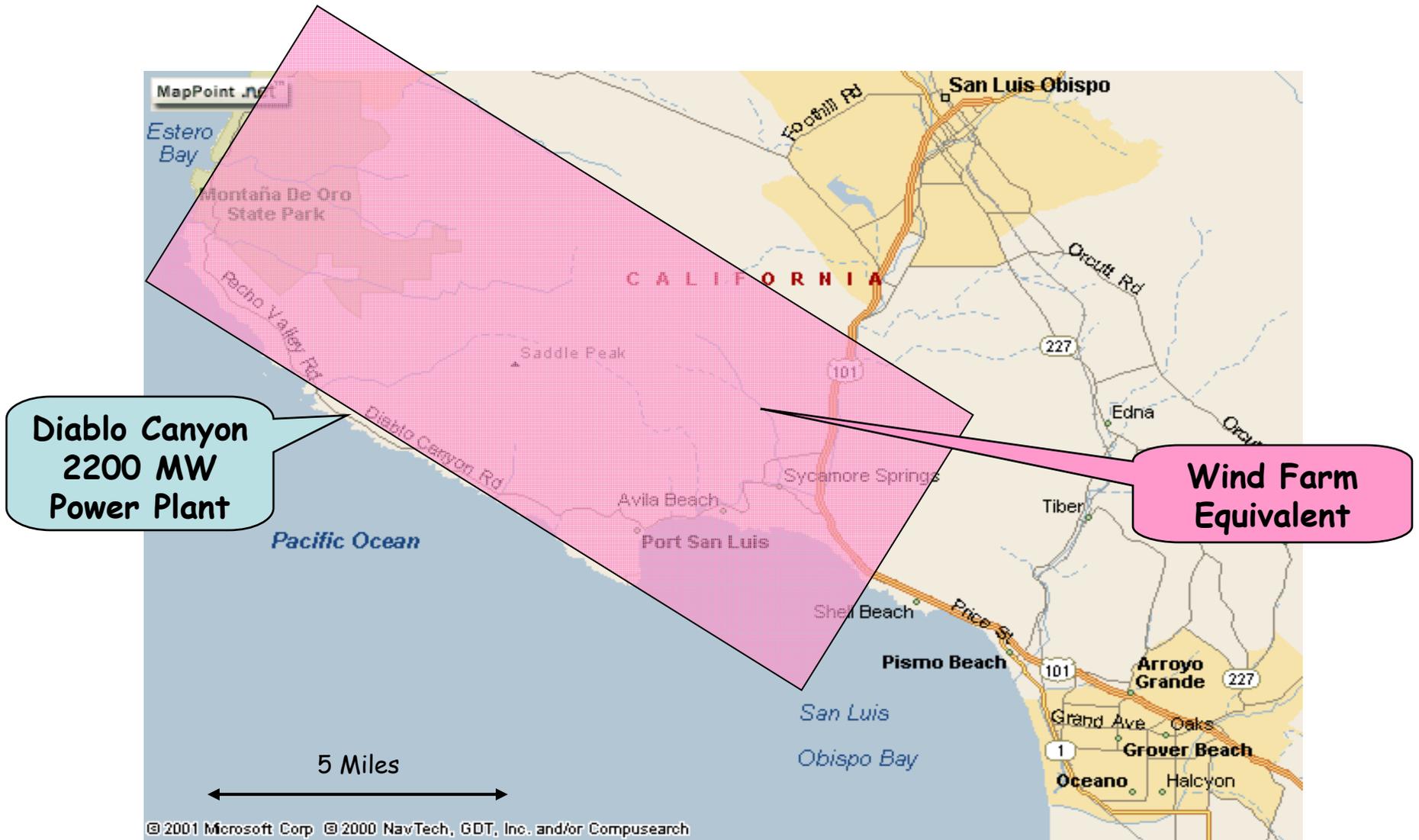
- You have to make it, just like electricity
- Electricity can make  $H_2$ , and  $H_2$  can make electricity ( $2H_2O \rightleftharpoons 2H_2 + O_2$ )
- You have to make a lot of it
- You can make it cold, - 419 F (21 K)

P.M. Grant, "Hydrogen lifts off...with a heavy load," *Nature* 424, 129 (2003)

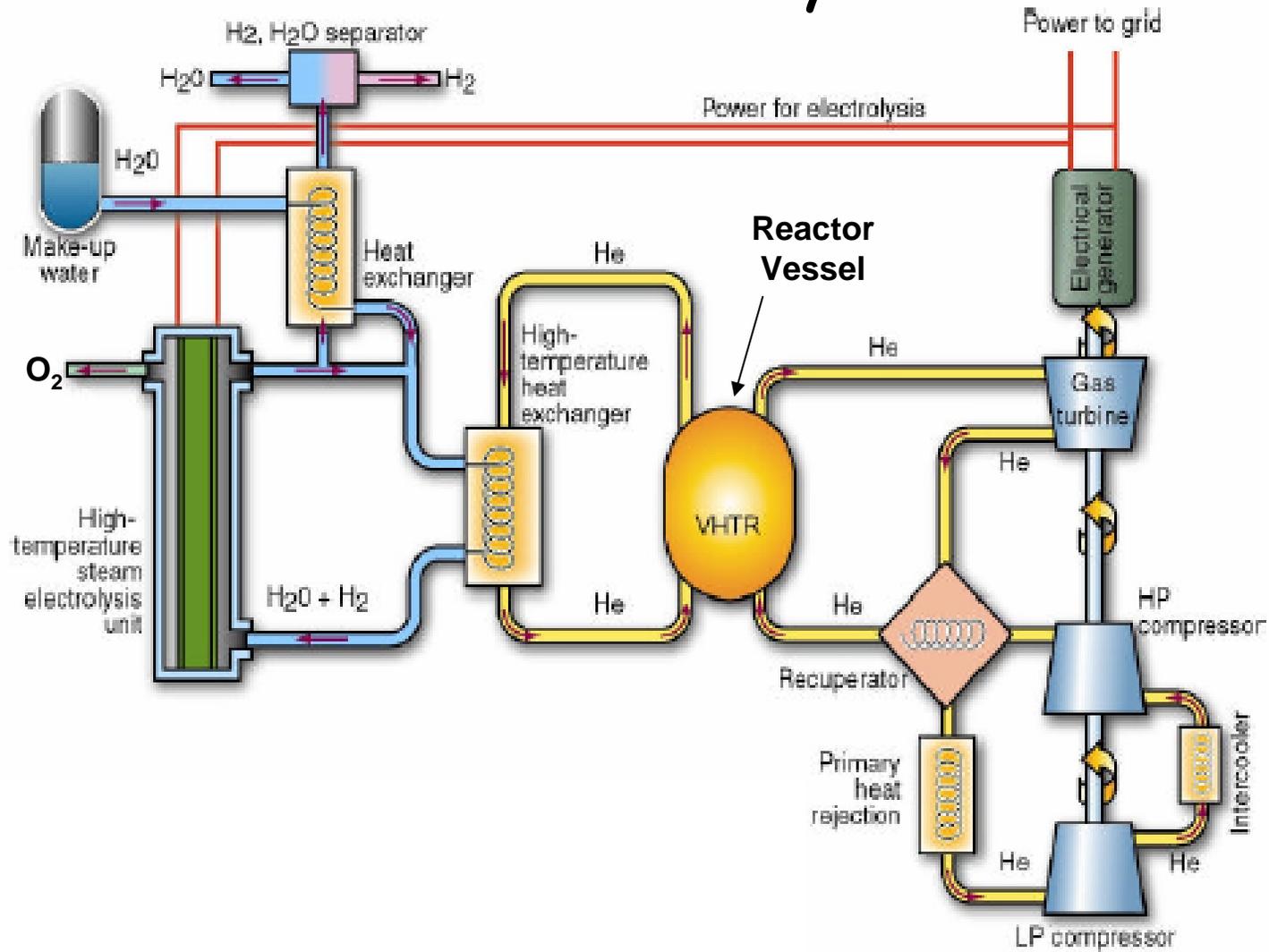
# Diablo Canyon



# California Coast Power

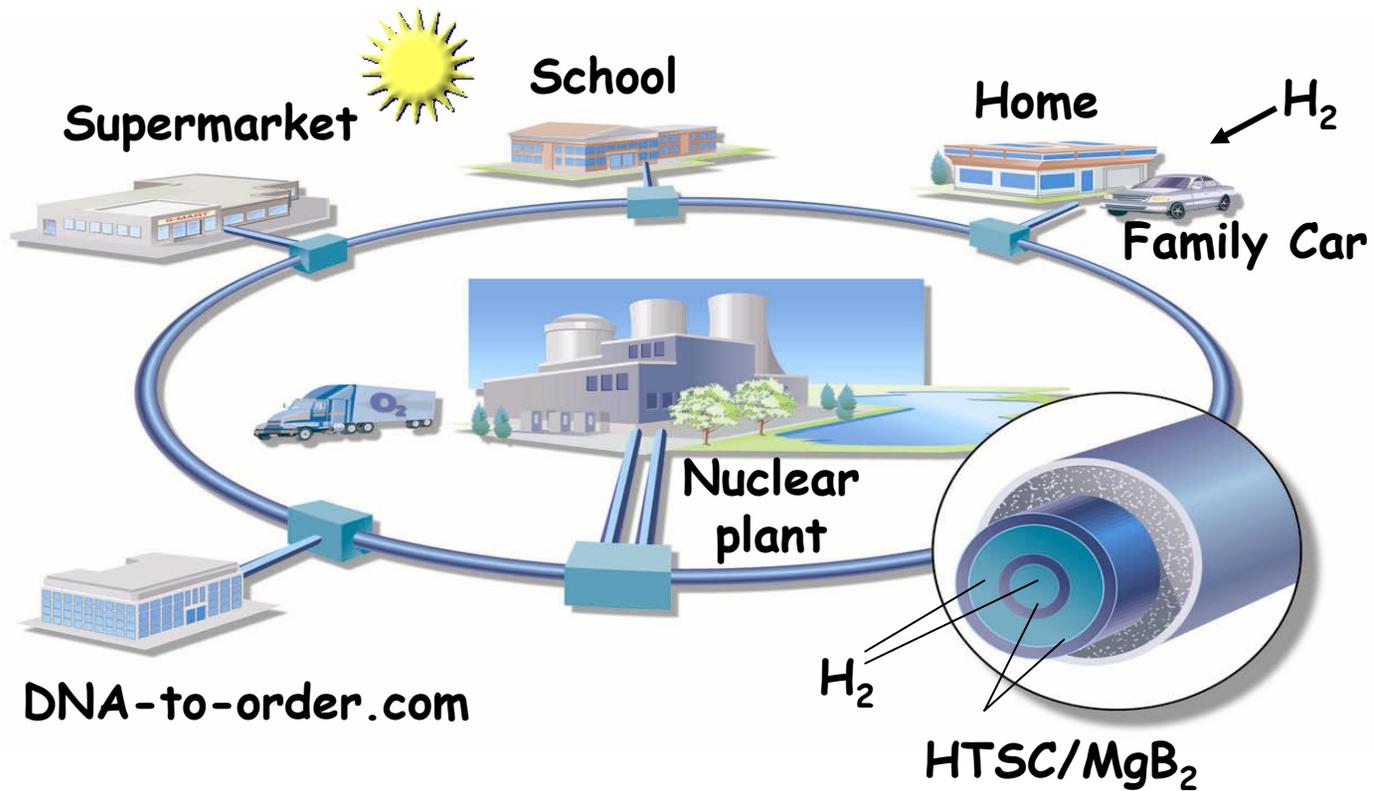


# Co-Production of Hydrogen and Electricity



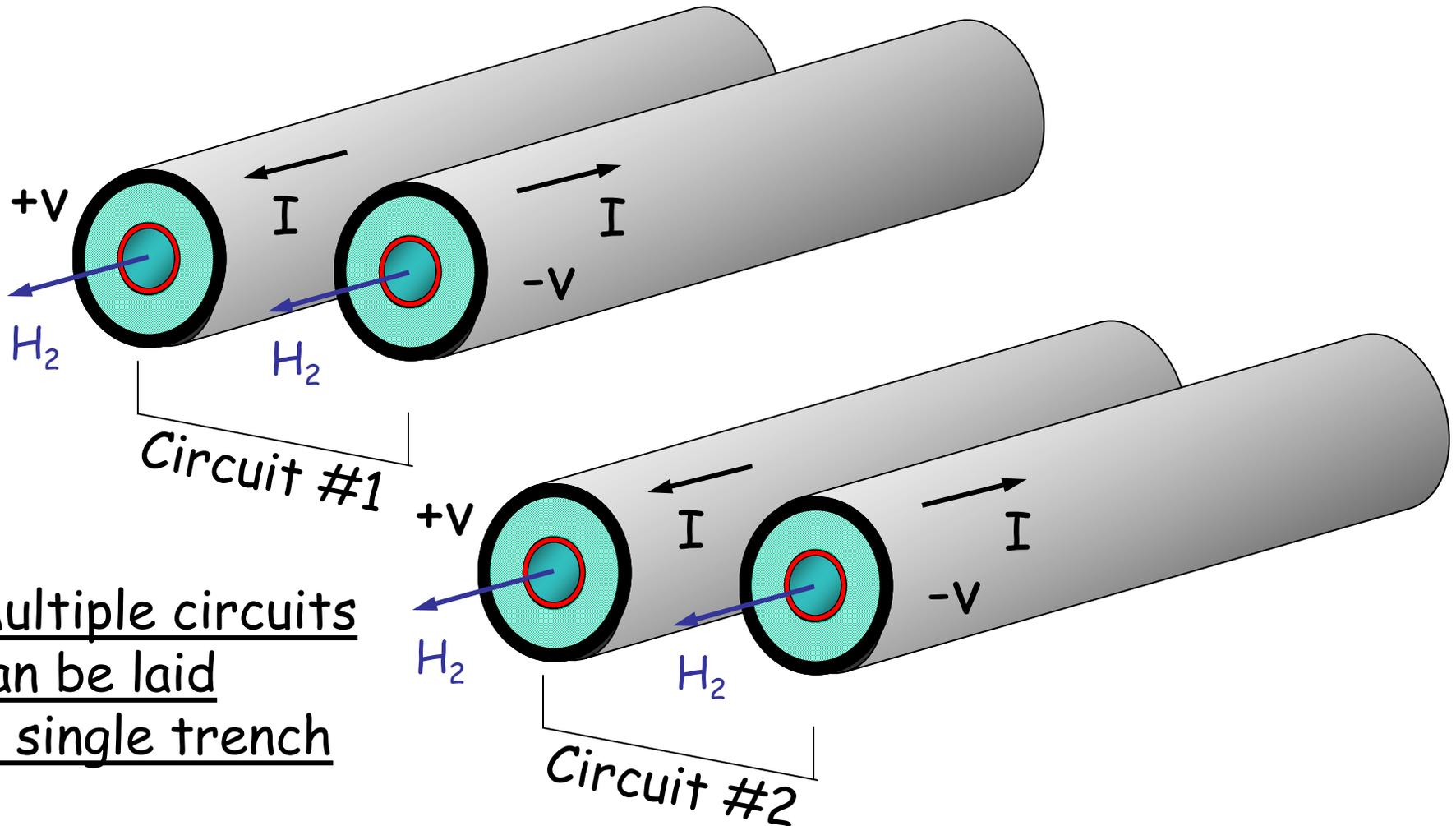
Source: INEL & General Atomics

# SuperCity



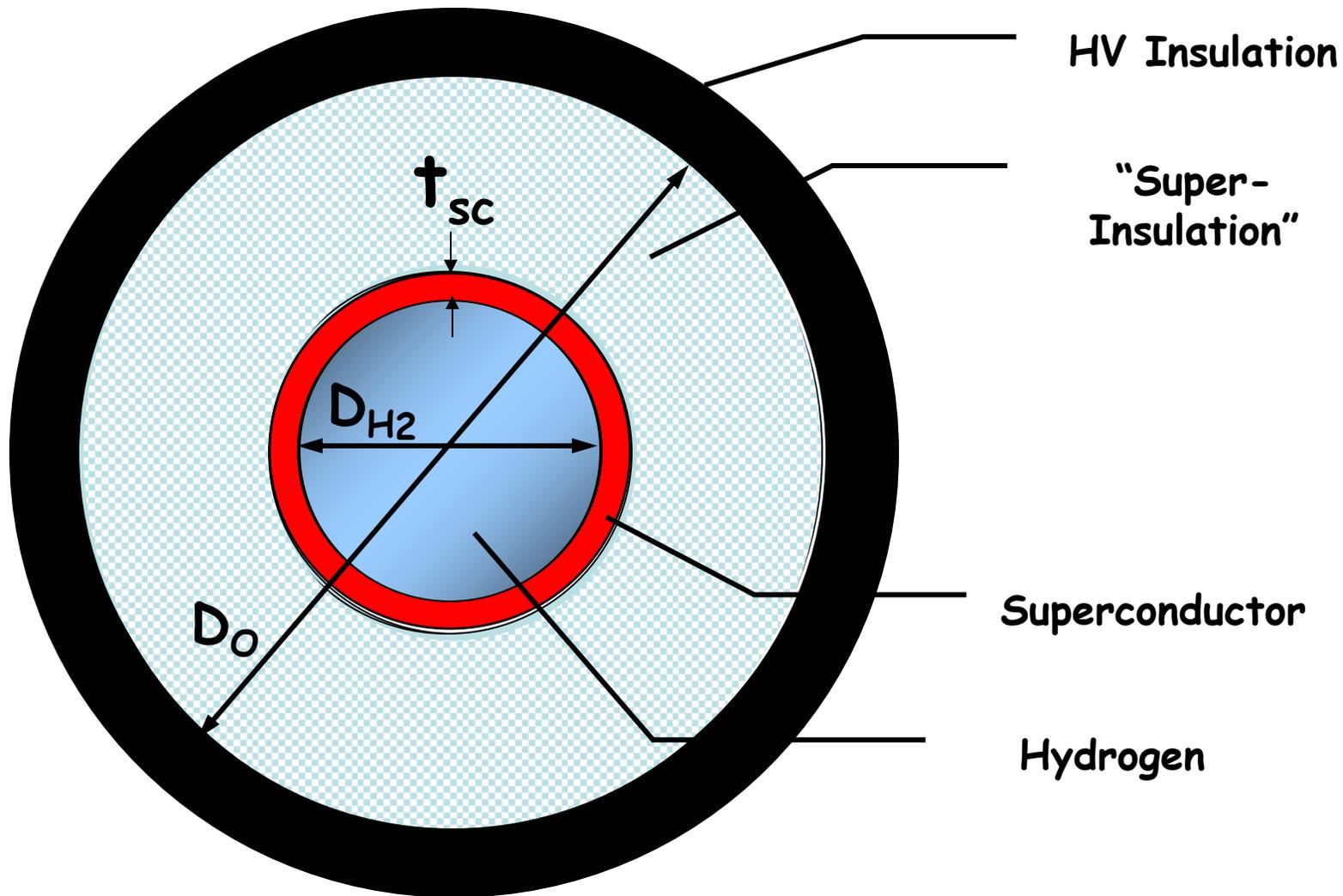
P.M. Grant, The Industrial Physicist, Feb/March Issue, 2002

# "Hydricity" SuperCables



Multiple circuits  
can be laid  
in single trench

# SuperCable Monopole



# Power Flows

$$P_{SC} = 2|V|IA_{SC}, \text{ where}$$

Electricity

$P_{SC}$  = Electric power flow

$V$  = Voltage to neutral (ground)

$I$  = Supercurrent

$A_{SC}$  = Cross-sectional area of superconducting annulus

$$P_{H_2} = 2(Q\rho vA)_{H_2}, \text{ where}$$

Hydrogen

$P_{H_2}$  = Chemical power flow

$Q$  = Gibbs  $H_2$  oxidation energy (2.46 eV per mol  $H_2$ )

$\rho$  =  $H_2$  Density

$v$  =  $H_2$  Flow Rate

$A$  = Cross-sectional area of  $H_2$  cryotube

# Hydricity Scaling Factor

Dimensionless, geometry-independent scaling factor defines relative amounts of electricity/hydrogen power flow in the SuperCable:

$$R_{e/h} \equiv (J / Q\rho)(|V| / v)$$

“Energy Density”

“Pressure”

# Electric & H<sub>2</sub> Power

## Electricity

Power (MW)	Voltage (V)	Current (A)	Critical Current Density (A/cm <sup>2</sup> )	Annular Wall Thickness (cm)
1000	+/- 5000	100,000	25,000	0.125

## Hydrogen (LH<sub>2</sub>, 20 K)

Power (MW)	Inner Pipe Diameter, D <sub>H2</sub> (cm)	H <sub>2</sub> Flow Rate (m/sec)	"Equivalent" Current Density (A/cm <sup>2</sup> )
500	10	3.81	318

# Thermal Losses

$$W_R = 0.5\varepsilon\sigma (T_{\text{amb}}^4 - T_{\text{SC}}^4), \text{ where}$$

$W_R$  = Power radiated in as watts/unit area

$$\sigma = 5.67 \times 10^{-12} \text{ W/cm}^2\text{K}^4$$

$$T_{\text{amb}} = 300 \text{ K}$$

$$T_{\text{SC}} = 20 \text{ K}$$

$\varepsilon = 0.05$  per inner and outer tube surface

$$D_{\text{SC}} = 10 \text{ cm}$$

$$W_R = 3.6 \text{ W/m}$$

Radiation  
Losses

Superinsulation:  $W_R^f = W_R/(n-1)$ , where

$n$  = number of layers

Target:  $W_R^f = \underline{0.5 \text{ W/m}}$  requires ~10 layers

Other addenda (convection, conduction):  $W_A = \underline{0.5 \text{ W/m}}$

$$W_T = W_R^f + W_A = \underline{1.0 \text{ W/m}}$$

# Heat Removal

$$dT/dx = W_T / (\rho v C_p A)_{H_2}, \text{ where}$$

$dT/dx$  = Temp rise along cable, K/m

$W_T$  = Thermal in-leak per unit Length

$\rho$  =  $H_2$  Density

$v$  =  $H_2$  Flow Rate

$C_p$  =  $H_2$  Heat Capacity

$A$  = Cross-sectional area of  $H_2$  cryotube

Take  $W_T = 1.0 \text{ W/m}$ , then  $dT/dx = 1.89 \times 10^{-5} \text{ K/m}$ ,

Or, 0.2 K over a 10 km distance

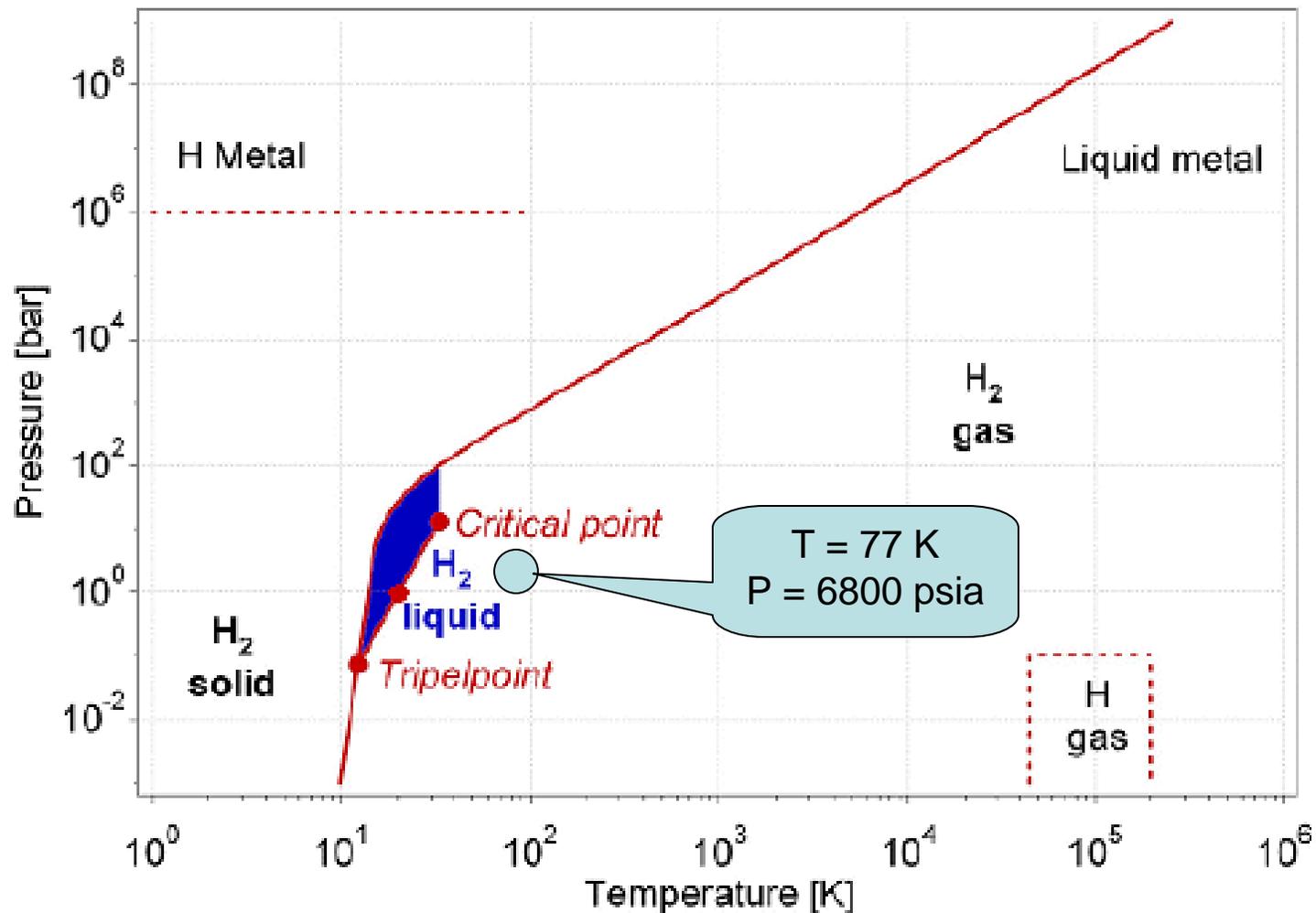
# SuperCable H<sub>2</sub> Storage

<u><i>Some Storage Factoids</i></u>	Power (GW)	Storage (hrs)	Energy (GWh)
TVA Raccoon Mountain	1.6	20	32
Alabama CAES	1	20	20
Scaled ETM SMES	1	8	8

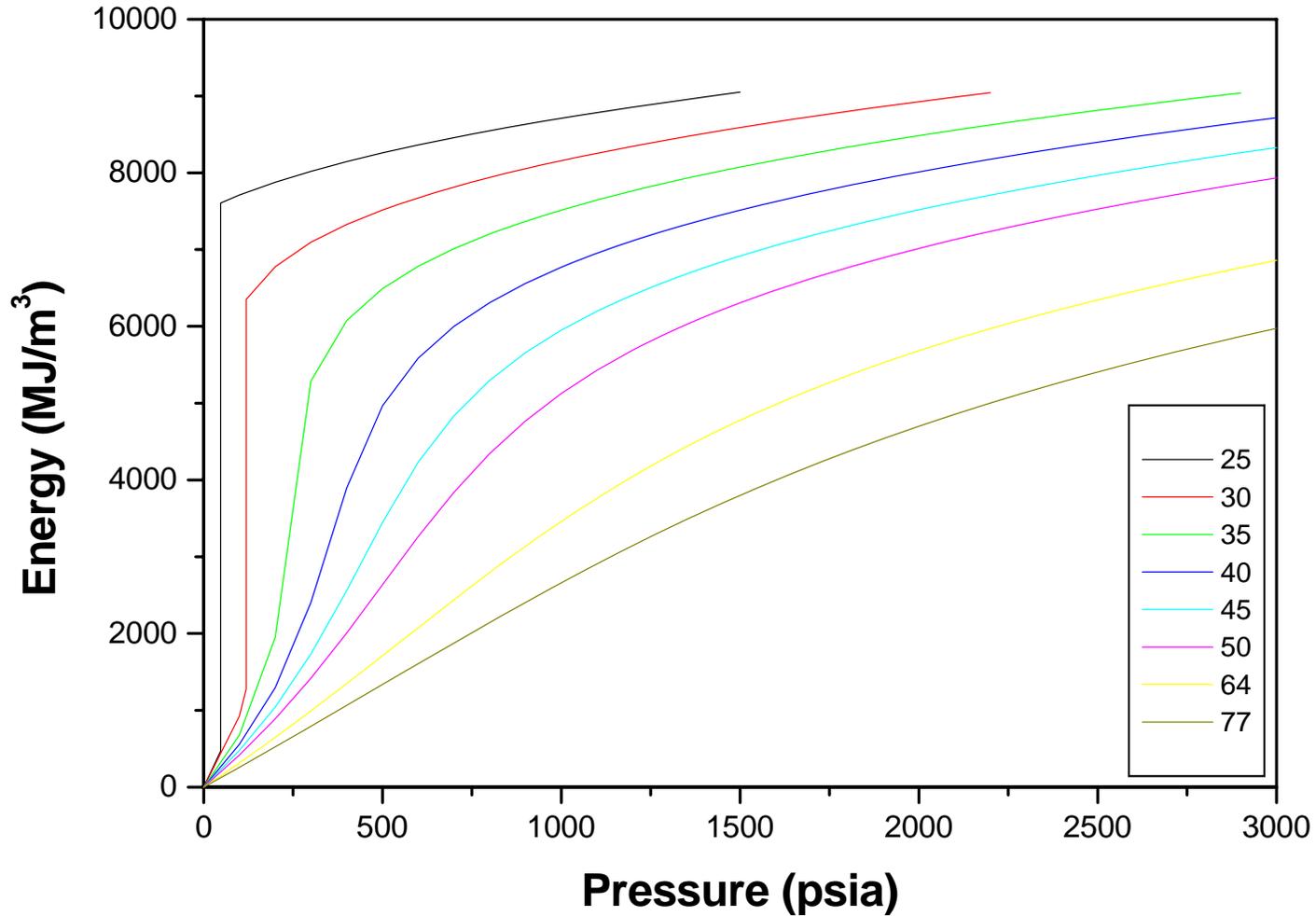
**One Raccoon Mountain = 13,800 cubic meters of LH<sub>2</sub>**

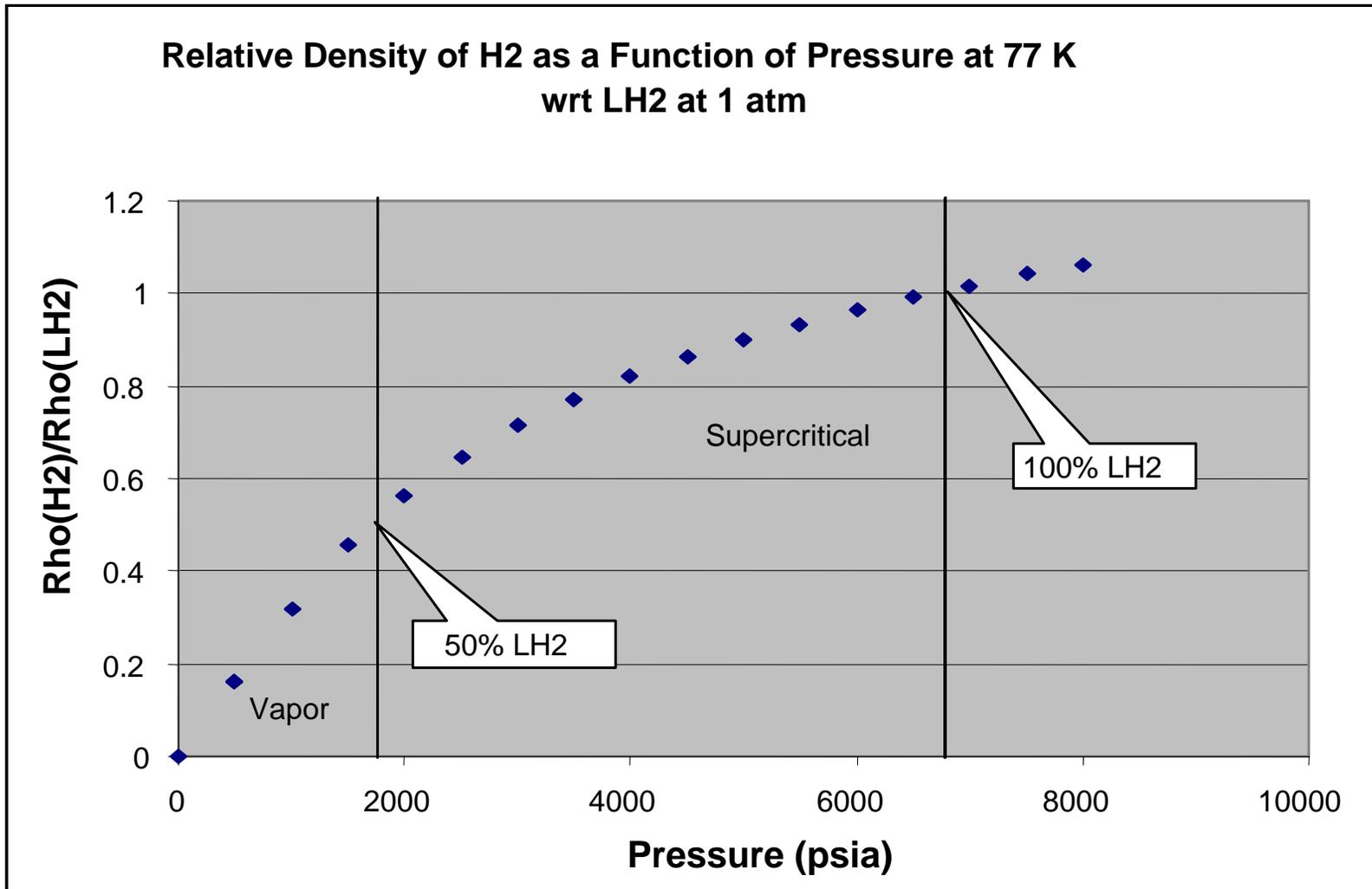
**LH<sub>2</sub> in 10 cm diameter, 250 mile bipolar SuperCable  
= Raccoon Mountain**

# Crude Phase Diagram of H<sub>2</sub>



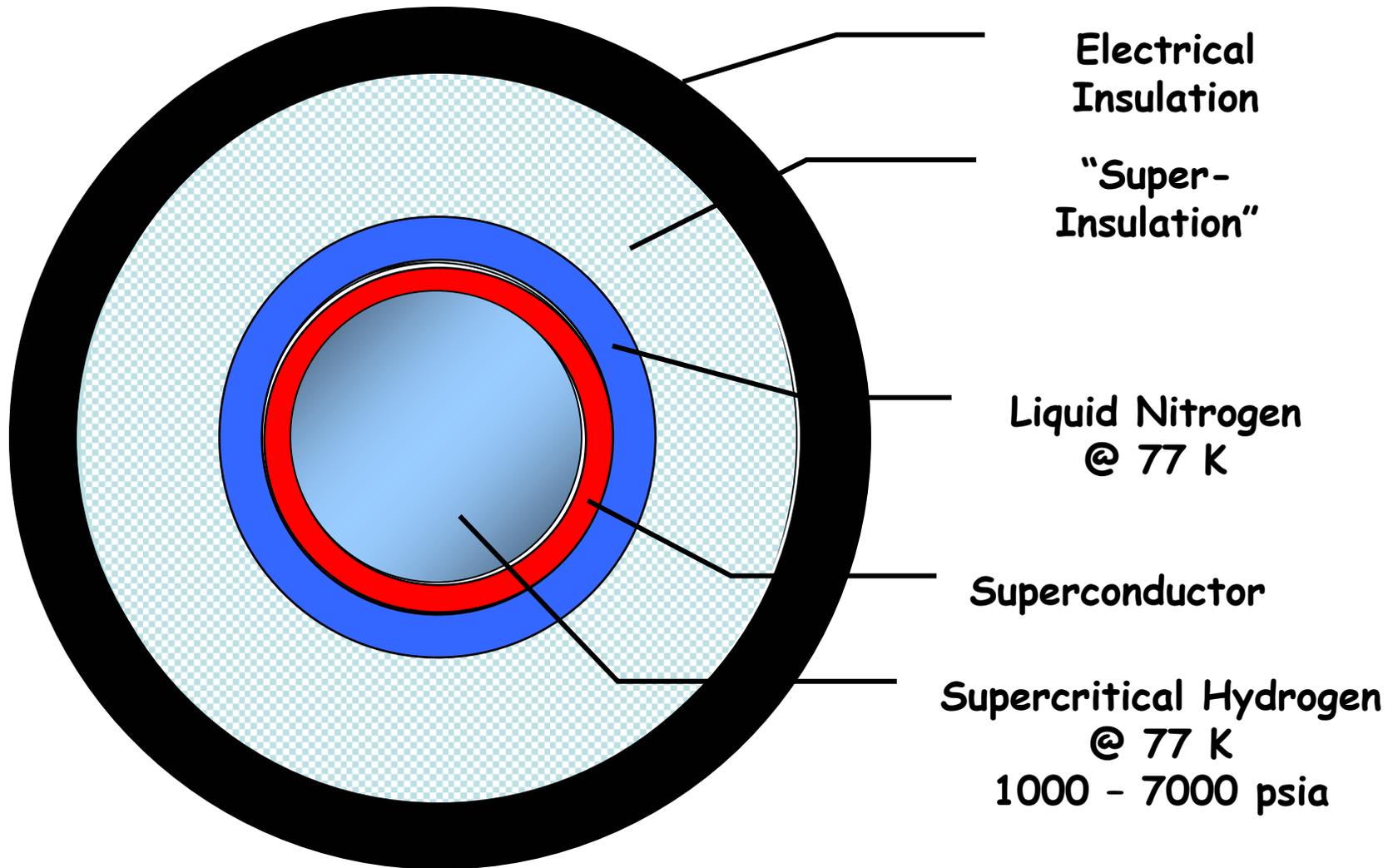
# Isothermal Properties of H<sub>2</sub>





**H<sub>2</sub> Gas at 77 K and 1850 psia has 50% of the energy content of liquid H<sub>2</sub> and 100% at 6800 psia**

# Supercritical H<sub>2</sub> SuperCable



## Fluid Properties Comparison of Liquid to Gaseous Hydrogen Transporting 500 MW<sub>t</sub> in a 10-cm Diameter Pipe

T °K	P psia	ρ kg/m <sup>3</sup>	μ μPa·s	μ <sup>2</sup> /ρ ndyne	V m/s	Re 10 <sup>6</sup>
20	14.7	70.8	13.6	261	4	2.08
77	1850	35.4	5.6	87	8	5.06

$$Re = \rho V D / \mu \approx \frac{\text{Inertial Forces}}{\text{Viscous Forces}}$$

*Thus, it takes only 0.5 dynes “push” on an object with the above Reynolds Numbers on the gas to overcome viscous forces exerted by the given fluid*

# Fluid Friction Losses

$$P_{loss} = \lambda (l / d_h) (\rho v^2 / 2)$$

where

$P_{loss}$  = pressure loss (Pa, N/m<sup>2</sup>)

$\lambda$  = friction coefficient

$l$  = length of duct or pipe (m)

$d_h$  = hydraulic diameter (m)

$$W_{loss} = M P_{loss} / \rho,$$

Where  $M$  = mass flow per unit length

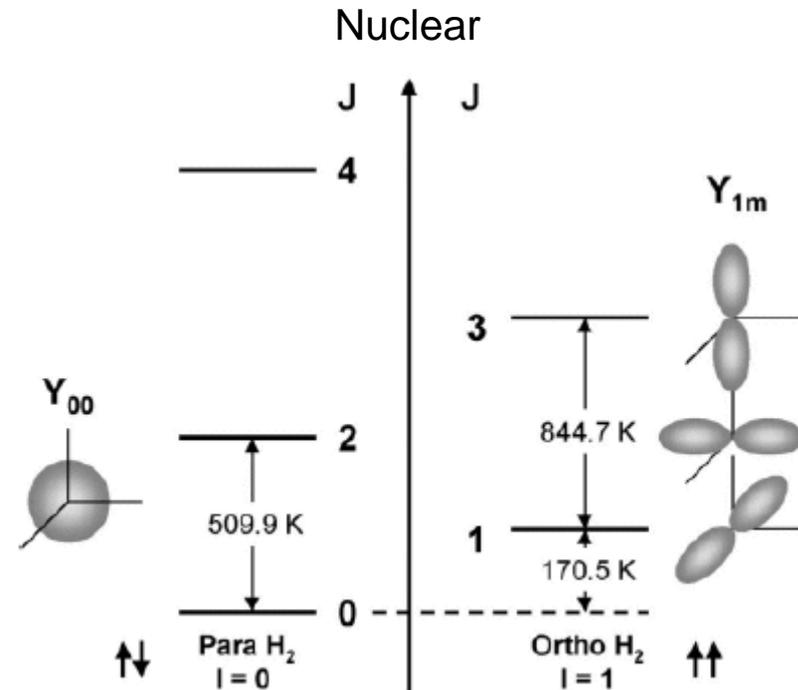
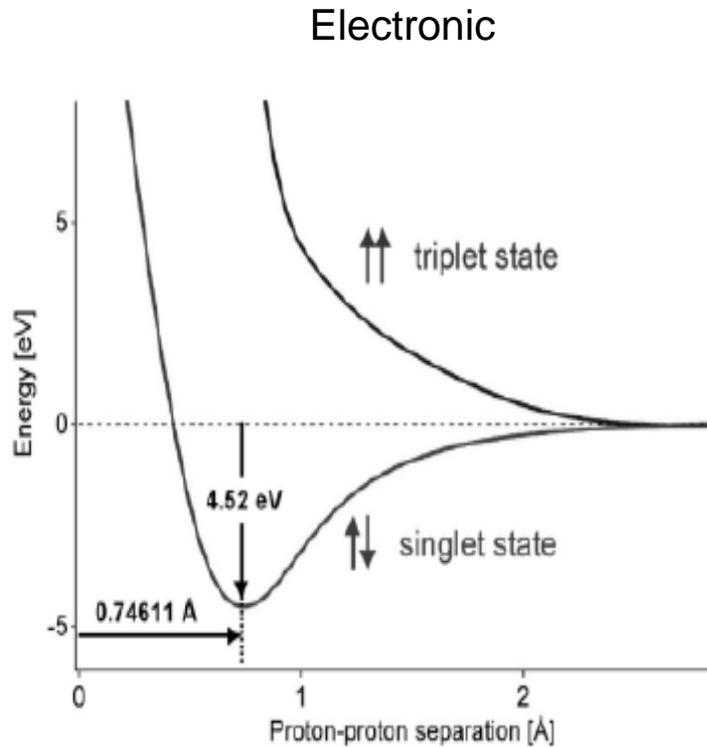
$P_{loss}$  = pressure loss per unit length

$\rho$  = fluid density

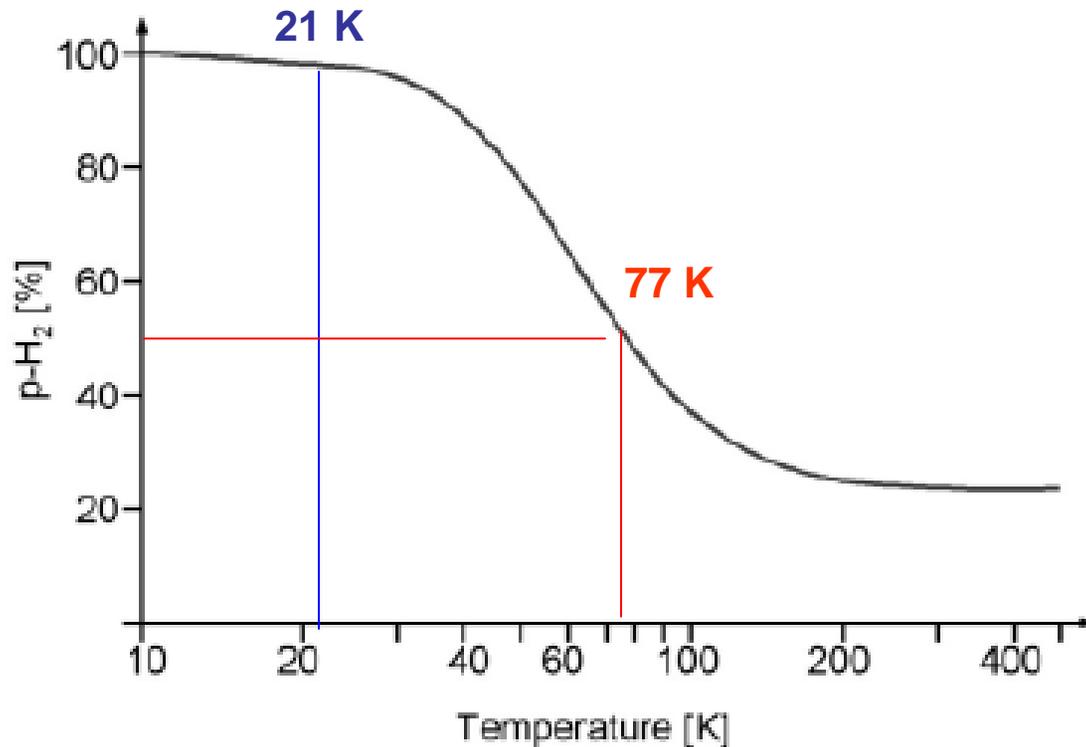
$$1 / \lambda^{1/2} = -2,0 \log_{10} [ (2,51 / (Re \lambda^{1/2})) + (\epsilon / d_h) / 3,72 ]$$

$\epsilon = 0.015$ mm (stainless steel)	
	$W_{loss}$ (W/m)
22 K	0.72
77 K	1.30

# Singlet (Para) - Triplet (Ortho) H<sub>2</sub>



# % para-H<sub>2</sub> in Normal H<sub>2</sub>

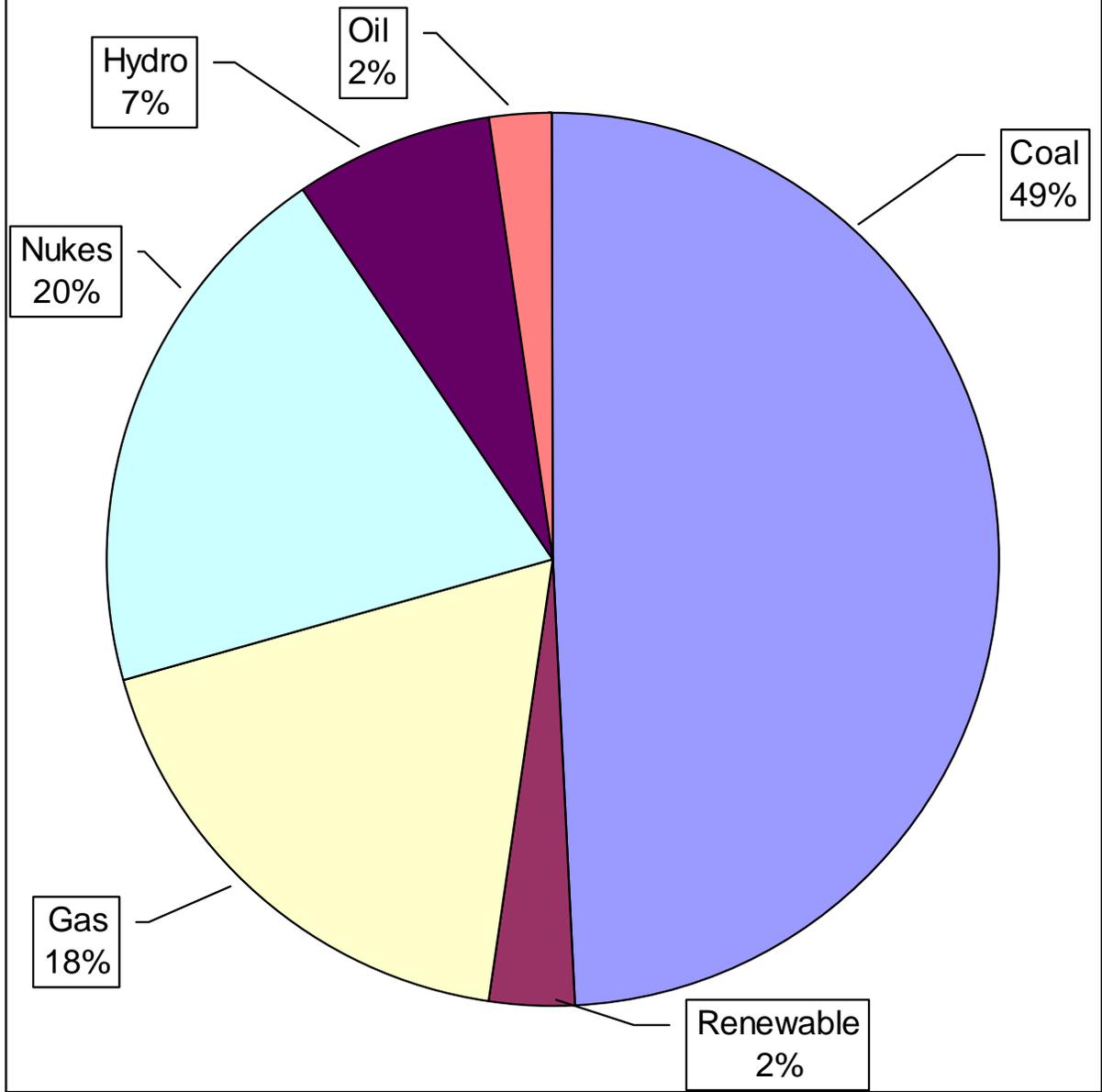


$$\frac{N_o}{N_p} = \frac{(I+1) \cdot \sum_{J=\text{odd}} q_J^r}{I \cdot \sum_{J=\text{even}} q_J^r} \quad \text{with } q_J^r = (2J+1) \cdot \exp\left\{-\frac{2 \cdot h^2}{8 \cdot \pi^2 M \cdot r_0^2} \frac{J(J+1)}{k \cdot T}\right\}$$

# An Unanswered Question (?)

- Is the para-ortho ratio dependent on magnetic field?
  - The peripheral field from a 100 kA superconductor cable can reach 1 T or greater.
  - Will this magnitude field induce a para-to-ortho spin flip? (maybe to 100% ortho?)
- At 77 K, H<sub>2</sub> is 50/50 para/ortho, and the ortho-para transition is exothermic with an enthalpy release of 523 kJ/kg.
- *Would a loss of electric current with concurrent magnetic field collapse result in an ortho-para transition and subsequent heating?*

### Electricity Generation - June 2004



# A Canadian's View of the World



# The Mackenzie Valley Pipeline

<http://www.mackenziegasproject.com>



**Mackenzie  
Delta**

**1220 km**

**18 GW-thermal**

**2006 - 2009**

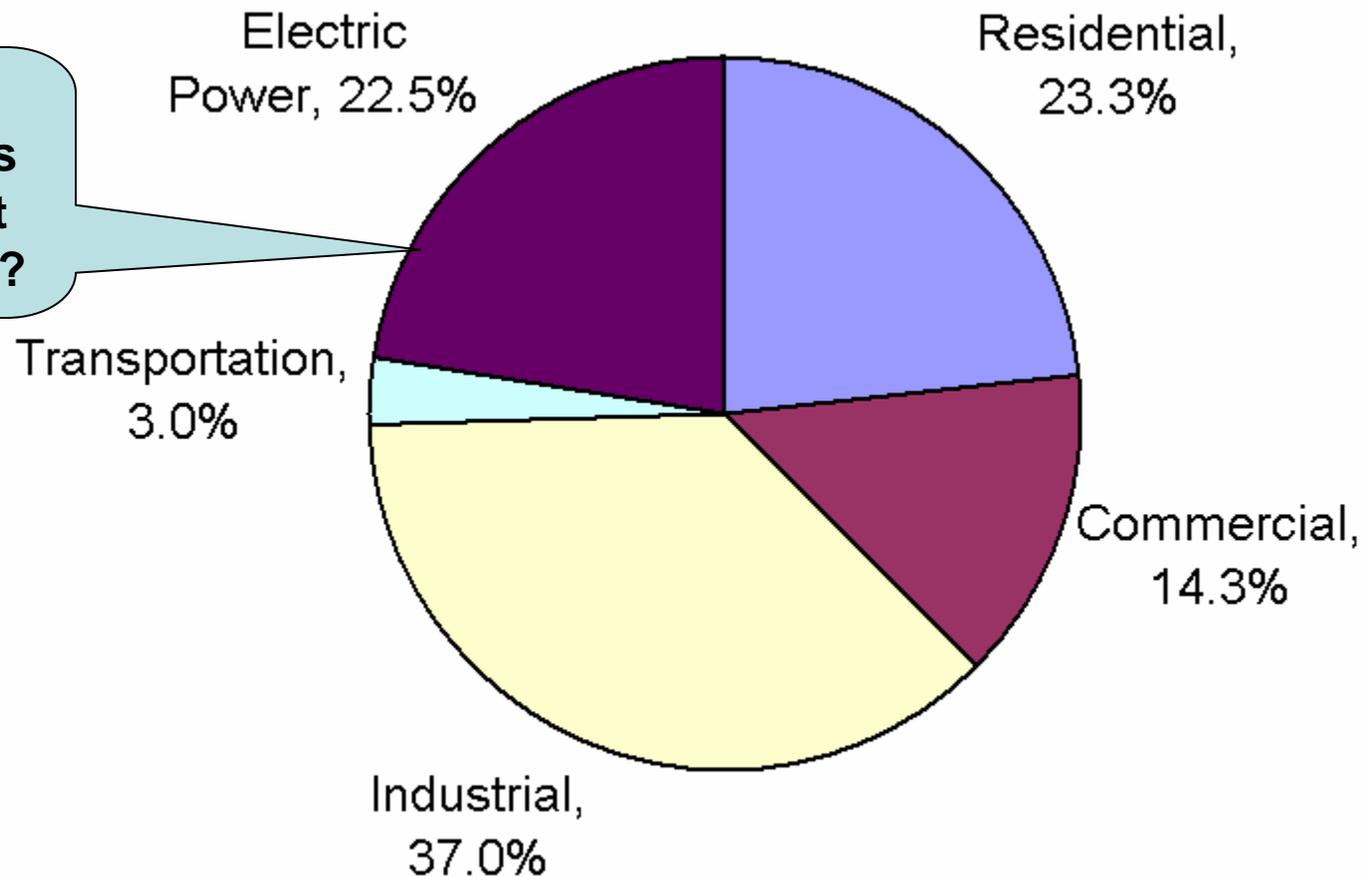
# MVP Specs

Pipeline Length	1220 km (760 mi)
Diameter	30 in (76 cm)
Gas Pressure	177 atm (2600 psia)
Pressurization Stations	~250 km apart
Flow Velocity	5.3 m/s (12 mph)
Mass Flow	345 kg/s
Volume Flow	1.6 Bcf/d (525 m <sup>3</sup> /s)
Power Flow	18 GW (HHV Thermal)
Construction Schedule	2006 - 2010
Employment	25,000
Partners	Esso, APG, C-P, Shell, Exxon
Cost	\$18 B (all private)

# 2004 Natural Gas End Use

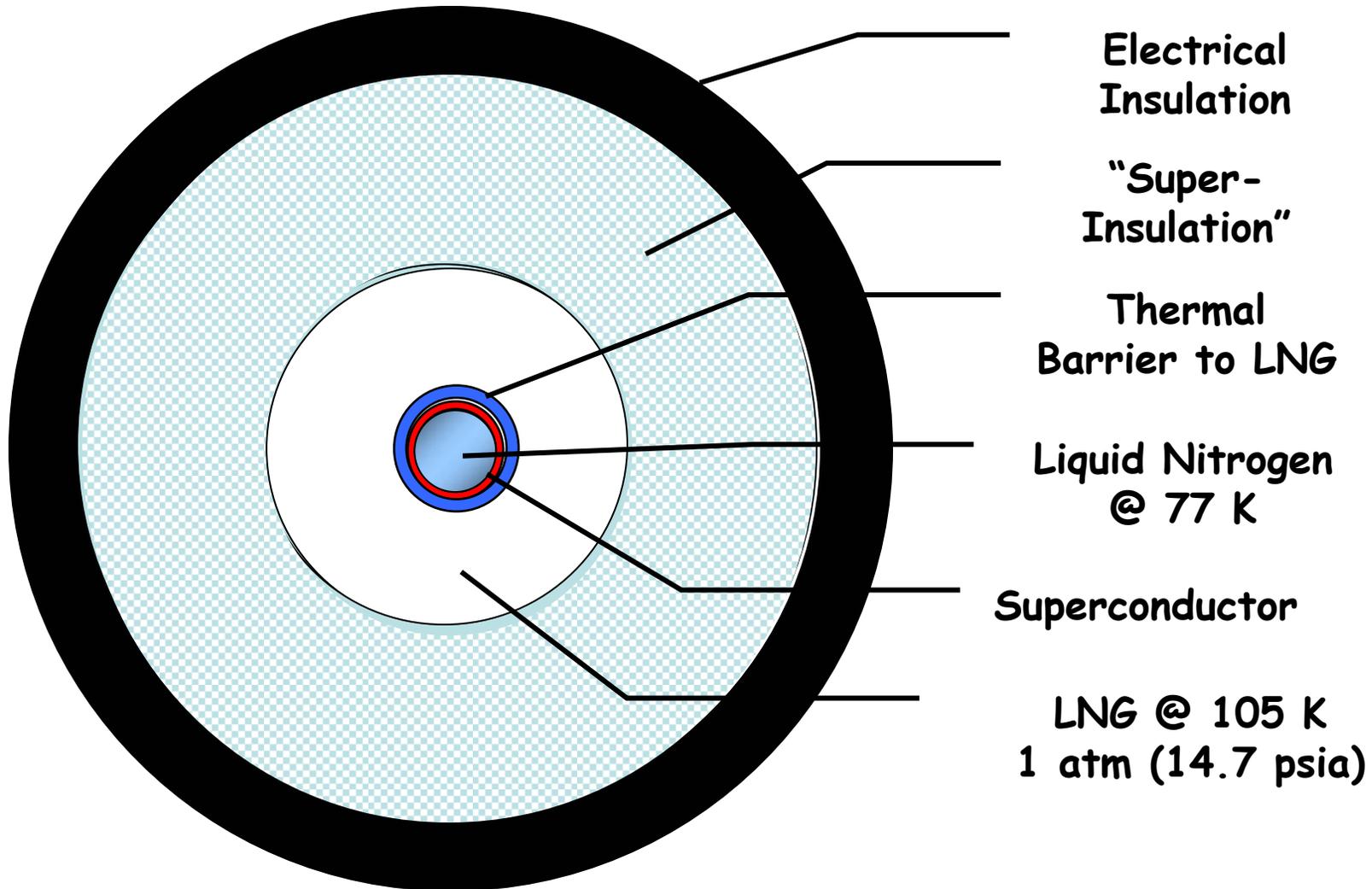
Schoenung, Hassenzahl and Grant, 1997  
(5 GW on HTSC @ LN<sub>2</sub>, 1000 km)

Why not  
generate this  
electricity at  
the wellhead?



Design for eventual  
conversion to high  
pressure cold or liquid  $H_2$

# LNG SuperCable



# MVP Wellhead Electricity

## Electricity Conversion Assumptions

Wellhead Power Capacity	18 GW (HHV)
Fraction Making Electricity	33%
Thermal Power Consumed	6 GW (HHV)
Left to Transmit as LNG	12 GW (HHV)
CCGT Efficiency	60%
Electricity Output	3.6 GW (+/- 18 kV, 100 kA)

## SuperCable Parameters for LNG Transport

CH <sub>4</sub> Mass Flow (12 GW (HHV))	230 kg/s @ 5.3 m/s
LNG Density (100 K)	440 kg/m <sup>3</sup>
LNG Volume Flow	0.53 m <sup>3</sup> /s @ 5.3 m/s
Effective Pipe Cross-section	0.1 m <sup>2</sup>
Effective Pipe Diameter	0.35 m (14 in)

# It's 2030

- *The Gas runs out!*
- Build HTCGR Nukes on the well sites in the Mackenzie Delta (some of the generator infrastructure already in place)
- Use existing LNG SuperCable infrastructure to transport protons and electrons
- Electricity/H<sub>2</sub> split needs to be determined...*Now!*

# LNG Danger To Our Communities Tim Riley Law .com 805-984-2350

Consumer Protection Attorney Tim Riley Warns About Liquefied Natural Gas

Certified Member of the Million Dollar Advocates Forum

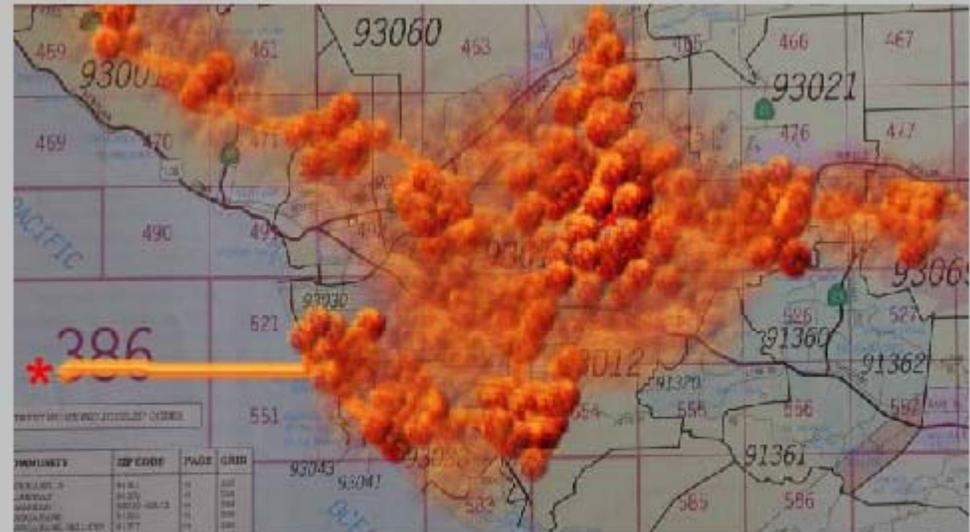
“The Top Trial Lawyers  
in the Country”



## Pipeline

Something Very Dangerous

“Underfoot”



PIPELINES A CONSTANT HAZARD!

# Take-Home Reading Assignment

[www.w2agz.com/cec-icmc05.htm](http://www.w2agz.com/cec-icmc05.htm)

1. Garwin and Matisoo, 1967 (100 GW on Nb<sub>3</sub>Sn)
2. Bartlit, Edeskuty and Hammel, 1972 (LH<sub>2</sub>, LNG and 1 GW on LTSC)
3. Haney and Hammond, 1977 (Slush LH<sub>2</sub> and Nb<sub>3</sub>Ge)
4. Schoenung, Hassenzahl and Grant, 1997 (5 GW on HTSC @ LN<sub>2</sub>, 1000 km)
5. Grant, 2003 ("Hydrogen Lifts Off...", Nature)
6. Grant, 2005 (The SuperCable)
7. SuperGrid Workshop, 2004 (See Bibliography)